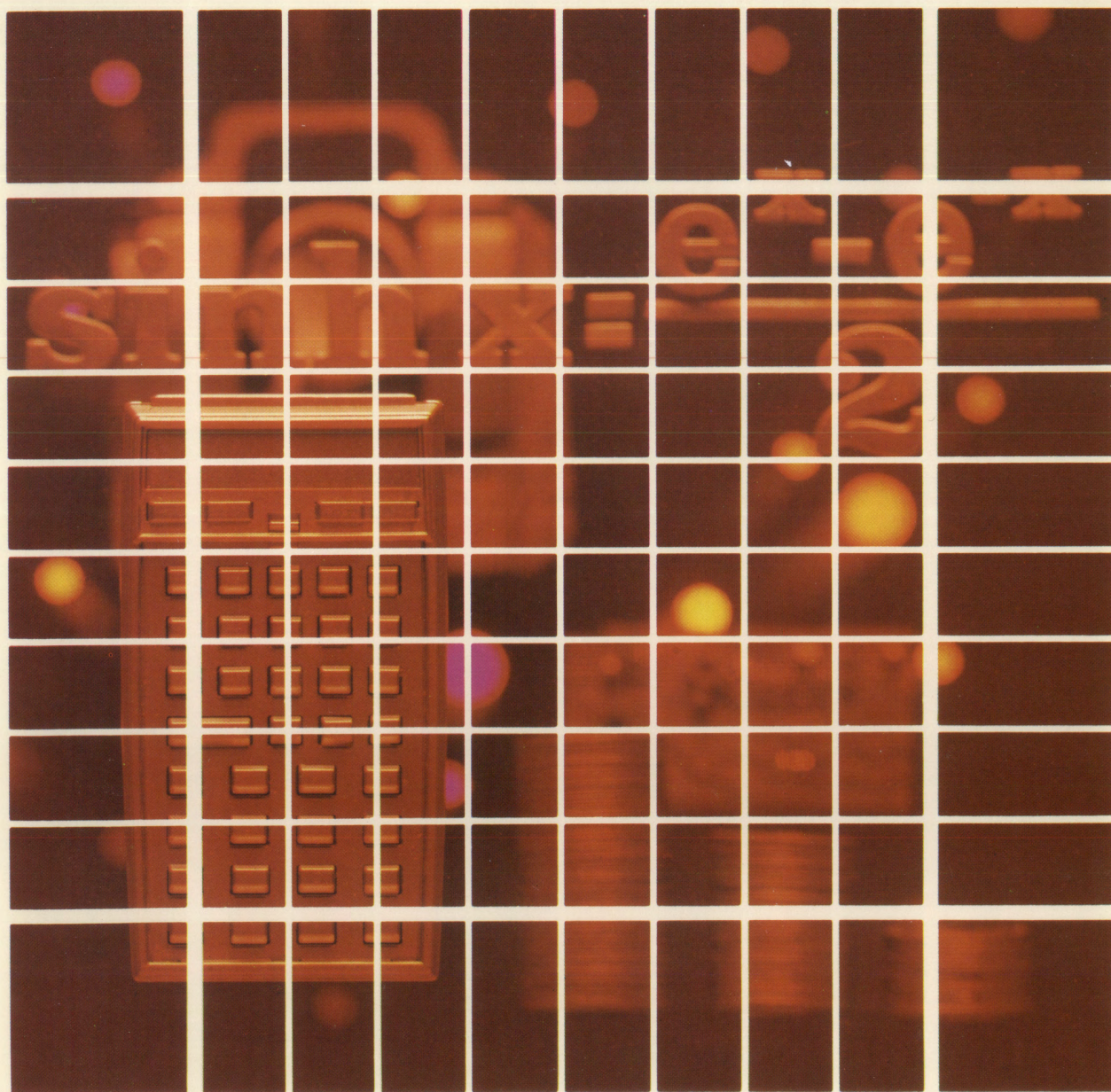


HEWLETT-PACKARD

HP-41C

USERS'
LIBRARY SOLUTIONS
Heating, Ventilating &
Air Conditioning



NOTICE

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INTRODUCTION

This HP-41C Solutions book was written to help you get the most from your calculator. The programs were chosen to provide useful calculations for many of the common problems encountered.

They will provide you with immediate capabilities in your everyday calculations and you will find them useful as guides to programming techniques for writing your own customized software. The comments on each program listing describe the approach used to reach the solution and help you follow the programmer's logic as you become and expert on your HP calculator.

KEYING A PROGRAM INTO THE HP-41C

There are several things that you should keep in mind while you are keying in programs from the program listings provided in this book. The output from the HP 82143A printer provides a convenient way of listing and an easily understood method of keying in programs without showing every keystroke. This type of output is what appears in this handbook. Once you understand the procedure for keying programs in from the printed listings, you will find this method simple and fast. Here is the procedure:

1. At the end of each program listing is a listing of status information required to properly execute that program. Included is the SIZE allocation required. Before you begin keying in the program, press **XEQ** **ALPHA** SIZE **ALPHA** and specify the allocation (three digits; e.g., 10 should be specified as 010).

Also included in the status information is the display format and status of flags important to the program. To ensure proper execution, check to see that the display status of the HP-41C is set as specified and check to see that all applicable flags are set or clear as specified.

2. Set the HP-41C to PRGM mode (press the **PRGM** key) and press **■** **GTO** **◻** **◻** to prepare the calculator for the new program.

3. Begin keying in the program. Following is a list of hints that will help you when you key in your programs from the program listings in this handbook.

- a. When you see " (quote marks) around a character or group of characters in the program listing, those characters are ALPHA. To key them in, simply press **ALPHA** , key in the characters, then press **ALPHA** again. So "SAMPLE" would be keyed in as **ALPHA** "SAMPLE" **ALPHA** .

- b. The diamond in front of each LBL instruction is only a visual aid to help you locate labels in the program listings. When you key in a program, ignore the diamond.

- c. The printer indication of divide sign is /. When you see / in the program listing, press **◻** **+** .

- d. The printer indication of the multiply sign is ✖ . When you see ✖ in the program listing, press **◻** **x** .

- e. The † character in the program listing is an indication of the **APPEND** function. When you see †, press **■** **APPEND** in ALPHA mode (press **■** and the K key).

- f. All operations requiring register addresses accept those addresses in these forms:

nn (a two-digit number)

IND nn (INDIRECT: **■** , followed by a two-digit number)

X, Y, Z, T, or L (a STACK address: **◻** followed by X, Y, Z, T, or L)

IND X, Y, Z, T or L (INDIRECT stack: **■** **◻** followed by X, Y, Z, T, or L)

Indirect addresses are specified by pressing **■** and then the indirect address. Stack addresses are specified by pressing **◻** followed by X, Y, Z, T, or L. Indirect stack addresses are specified by pressing **■** **◻** and X, Y, Z, T, or L.

Printer Listing

```

01♦LBL "SAM
PLE"
02 "THIS IS
A "
03 "†SAMPLE
"
04 AVIEW
05 6
06 ENTER†
07 -2
08 /
09 ABS
10 STO IND
L
11 "R3="
12 ARCL 03
13 AVIEW
14 RTN
    
```

Keystrokes

```

■ LBL ALPHA SAMPLE ALPHA
ALPHA THIS IS A ALPHA
ALPHA ■ APPEND SAMPLE
■ AVIEW ALPHA
6
ENTER†
2 CHS
+
XEQ ALPHA ABS ALPHA
STO ■ ◻ L
ALPHA R3= ■ ARCL 03
■ AVIEW
ALPHA
■ RTN
    
```

Display

```

01 LBLT SAMPLE
02T THIS IS A
03T † SAMPLE
04 AVIEW
05 6
06 ENTER ↗
07 -2
08 /
09 ABS
10 STO IND L
11T R3=
12 ARCL 03
13 AVIEW
14 RTN
    
```


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	Given economic and engineering parameters, computes the years to break even on an insulation investment.	
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	Computes properties of moist air based on temperature, pressure and either wet bulb temperature, relative humidity, or vapor pressure.	
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	Correlates heat transfer for counterflow, parallel flow, parallel-counterflow and crossflow heat exchangers.	
9.	DECIBEL ADDITION AND SUBTRACTION	65
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10.	TEMPERATURE CONVERSIONS	69
	Converts interchangeably between Kelvin, Fahrenheit, Celsius, and Rankin.	

* These programs require one memory module.

** This program requires two memory modules.

OVERALL HEAT TRANSFER COEFFICIENTS

This program sums convective and conductive coefficients to obtain the overall heat transfer coefficient for walls.

Equations:

$$U = \frac{1}{R_0 + R_1 + R_2 + \dots + R_n + \frac{1}{h_0} + \frac{1}{h_1} + \frac{1}{h_2} + \dots + \frac{1}{h_n} + \frac{x}{k_0} + \frac{x}{k_1} + \frac{x}{k_2} + \dots + \frac{x}{k_n} + \frac{1}{C_0} + \frac{1}{C_1} + \frac{1}{C_2} + \dots + \frac{1}{C_n}}$$

where:

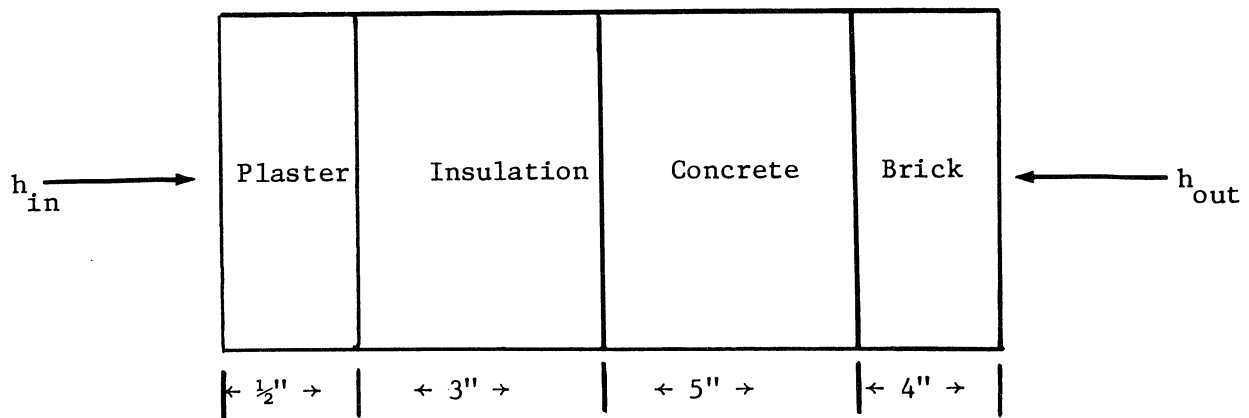
- Q is the heat transfer
- U is the overall heat transfer coefficient
- ΔT is the temperature difference across the wall
- R is the thermal resistance of a layer in the wall
- h is the convective resistance at a surface of the wall
- x is the thickness of a conductive layer
- k is the thermal conductivity of a substance
- C is the thermal conductance of a layer

Reference:

Threlkeld, James L.; Thermal Environmental Engineering; Prentice-Hall, Inc. 1970

Example:

What is the overall heat transfer coefficient for the wall below? What is the heat transfer for a 20°F temperature difference?



Layer	Coefficient	Symbol	Units
Inside Air	1.46	h	B/(hr) (ft ²) (°F)
Plaster	5	k	B/(hr) (ft ²) (°F/in)
Insulation	11	R	(hr) (ft ²) (°F)/BTU
Concrete	12	h	BTU/(hr) (ft ²) (°F/in)
Brick	36	C	BTU/(hr) (ft ²) (°F)
Outside Air	6	h	BTU/(hr) (ft ²) (°F)

Keystrokes:

[///] [FIX] 4
[XEQ] [ALPHA] HEAT [ALPHA]
1.46 [A]
.5 [ENTER ↑] 5 [B]
11 [D]
5 [ENTER ↑] 12 [B]
36 [C]
6 [A]
[R/S]
20 [x]

Display:

H X↑K C R CL
H X↑K C R CL
H X↑K C R CL
H X↑K C R CL
H X↑K C R CL
H X↑K C R CL
H X↑K C R CL
U=0.0807
1.6134 (Btu/(ft²)(hr))

Program Listings

<pre> 01*LBL "HEA T" 02*LBL E 03 ADV 04 SF 27 05 CLST 06*LBL 01 07 "H X↑K C R CL" 08 PROMPT 09 ADV 10 "U=" 11 ARCL X 12 SF 21 13 AVIEW 14 GTO 01 15*LBL A 16 "H" 17 XEQ 00 18 1/X 19 GTO 02 20*LBL B 21 "X=" 22 ARCL Y 23 FS? 55 24 PRA 25 "K" 26 XEQ 00 27 / 28 GTO 02 29*LBL C 30 "C" 31 XEQ 00 32 1/X 33 GTO 02 34*LBL D 35 "R" 36 XEQ 00 37*LBL 02 38 RCL Y 39 X≠0? 40 1/X 41 + 42 1/X 43 GTO 01 44*LBL 00 45 "f=" 46 ARCL X 47 FS? 55 48 PRA 49 RTN </pre>	<p>Initialize program.</p> <p>Define keyboard.</p> <p>Output U.</p> <p>Add convective coefficient.</p> <p>Add conductive coefficient.</p> <p>Add conductance.</p> <p>Add resistance.</p> <p>Print input.</p>	<p>51</p> <p>60</p> <p>70</p> <p>80</p> <p>90</p> <p>00</p>	
---	--	---	--

REGISTERS, STATUS, FLAGS, ASSIGNMENTS

DATA REGISTERS			STATUS				
00		50	SIZE	ANY	TOT. REG.	15	USER MODE
			ENG		FIX	SCI	ON <input checked="" type="checkbox"/> OFF
			DEG		RAD	GRAD	
05		55	FLAGS				
			#	INIT S/C	SET INDICATES	CLEAR INDICATES	
10		60					
15		65					
20		70					
25		75					
30		80					
35		85					
			ASSIGNMENTS				
			FUNCTION	KEY	FUNCTION	KEY	
40		90					
45		95					

INSULATION BREAK EVEN ANALYSIS

This program calculates the number of years necessary for insulation to pay for itself based on heating costs. Inflation and the cost of money are accounted for.

Equations:

$$\text{YEARS} = \frac{-\ln \left(1 - \frac{\$/\text{FT}^2 (\% \text{INT} - \% \text{INF})}{\text{Yearly Savings}} \right)}{\ln \left(1 + \frac{\% \text{INT} - \% \text{INF}}{1 + \% \text{INF}} \right)}$$

$$\text{YEARLY SAVINGS} = \left(U - \frac{1}{(1/U + R)} \right) (\text{DEGDY}) (24) (\$/\text{BTU})$$

where:

YEARS is the number of years before insulation pays for itself.

$\$/\text{FT}^2$ is the cost of the insulation on a square foot basis.

%INT is the current lending rate to obtain insulation.

%INF is the expected inflation rate for the heat source being considered.

U is the overall heat transfer coefficient for the surface being considered with no insulation installed, $\text{Btu}/(\text{hr})(\text{ft}^2)(^\circ\text{F})$.

R is the thermal resistance of the insulating material, $(\text{hr})(\text{ft}^2)(^\circ\text{F})/\text{BTU}$.

DEGDY is the number of degree days for the area being considered.
See the ASHRAE GUIDE AND DATA BOOK for degree day information.

$\$/\text{BTU}$ is the current cost of heat per Btu.

Example:

A home in Seattle, Washington, (5145 degree days per year) is to have walls insulated with either R11 or R19 insulation costing 0.25 or 0.40 dollars per square foot respectively. The heat transfer coefficient for the un-insulated walls is $0.28 \text{ Btu}/(\text{hr})(\text{ft}^2)(^\circ\text{F})$. Natural gas at a cost of $3.66 \times 10^{-6} \text{ \$/Btu}$ is the heat source. Financing is available at 11% and energy is expected to inflate at 15% per year. How many years will it take for the two insulation choices to pay for themselves?

Keystrokes: (SIZE \geq 009)

Display:

[////] [FLX] 2

[XEQ] [ALPHA] INSUL [ALPHA]

.28 [R/S]

3.66 [EEX] [CHS] 6 [R/S]

11 [R/S]

15 [R/S]

5145 [R/S]

11 [R/S]

.25 [R/S]

[R/S]*

19 [R/S]

.4 [R/S]

[R/S]*

U=?

\$/BTU=?

% INT=?

% INF=?

DEGDY=?

R=?

\$/FT2=?

YEARS=2.81

R=?

\$/FT2

YEARS=3.95

R=?

*Press [R/S] if you are not using a printer.

Program Listings

<pre> 01*LBL "INS UL" 02 ADV 03 0 04 STO 00 05 "U" 06 XEQ "IN" 07 "\$/BTU" 08 XEQ "IN" 09 "%INT" 10 XEQ "IN" 11 "%INF" 12 XEQ "IN" 13 "DEGDY" 14 XEQ "IN" 15*LBL 01 16 5 17 STO 00 18 "R" 19 XEQ "IN" 20 "\$/FT2" 21 XEQ "IN" 22 RCL 01 23 RCL 01 24 1/X 25 RCL 06 26 + 27 1/X 28 - 29 RCL 05 30 * 31 RCL 02 32 * 33 24 34 * 35 RCL 03 36 RCL 04 37 - 38 X=0? 39 GTO 00 40 100 41 / 42 STO 08 43 / 44 RCL 07 45 X<>Y 46 / 47 CHS 48 LN1+X 49 CHS </pre>	<p>Input values.</p>	<pre> 50 RCL 08 51 RCL 04 52 100 53 / 54 1 55 + 56 / 57 LN1+X 58 / 59*LBL 03 60 ADV 61 "YEARS" 62 XEQ "0" 63 ADV 64 GTO 01 65*LBL 00 66 RDN 67 RCL 07 68 RCL 04 69 % 70 + 71 X<>Y 72 / 73 GTO 03 74*LBL "IN" 75 CF 22 76 1 77 ST+ 00 78 RCL IND 00 79 "F=" 80 ASTO Y 81 "F?" 82 CF 21 83 AVIEW 84 SF 21 85 CLA 86 ARCL Y 87 STOP 88 STO IND 00 89 FS? 22 90 FC? 55 91 RTN 92 ARCL X 93 PRA 94 RTN 95*LBL "0" 96 "F=" 97 ARCL X 98 AVIEW </pre>	<p>Output years.</p>
<pre> 22 RCL 01 23 RCL 01 24 1/X 25 RCL 06 26 + 27 1/X 28 - 29 RCL 05 30 * 31 RCL 02 32 * 33 24 34 * 35 RCL 03 36 RCL 04 37 - 38 X=0? 39 GTO 00 40 100 41 / 42 STO 08 43 / 44 RCL 07 45 X<>Y 46 / 47 CHS 48 LN1+X 49 CHS </pre>	<p>Calculate savings.</p>	<pre> 74*LBL "IN" 75 CF 22 76 1 77 ST+ 00 78 RCL IND 00 79 "F=" 80 ASTO Y 81 "F?" 82 CF 21 83 AVIEW 84 SF 21 85 CLA 86 ARCL Y 87 STOP 88 STO IND 00 89 FS? 22 90 FC? 55 91 RTN 92 ARCL X 93 PRA 94 RTN 95*LBL "0" 96 "F=" 97 ARCL X 98 AVIEW </pre>	<p>Special case where inflation equals interest.</p>
<pre> 35 RCL 03 36 RCL 04 37 - 38 X=0? 39 GTO 00 40 100 41 / 42 STO 08 43 / 44 RCL 07 45 X<>Y 46 / 47 CHS 48 LN1+X 49 CHS </pre>	<p>Calculate years.</p>	<pre> 95*LBL "0" 96 "F=" 97 ARCL X 98 AVIEW </pre>	<p>Input subroutine.</p> <p>Output subroutine.</p>

AIR FLOW IN CIRCULAR DUCTS

(Requires one memory module)

This program can be used to compute the pressure difference, velocity or volumetric flow rate for air in circular, metal, HVAC ducts.

Equations:

$$v^2 = \frac{dP/\rho}{2 \left(f \frac{L}{D} + \frac{K_T}{4} \right)}$$

For laminar flow ($Re < 2300$)

$$f = 16/Re$$

For turbulent flow ($Re > 2300$)

$$\frac{1}{\sqrt{f}} = 1.737 \ln \frac{D}{\epsilon} + 2.28 - 1.737 \ln \left(4.67 \frac{D}{\epsilon Re \sqrt{f}} + 1 \right)$$

is solved by Newton's method.

$$\frac{1}{\sqrt{f_0}} = 1.737 \ln \frac{D}{\epsilon} + 2.28$$

is used as an initial guess in the iteration.

$$\mu = 1.101 \times 10^{-6} (T)^{1.5} / (T+200) \text{ (N}\cdot\text{s/m}^2\text{)}$$

$$\rho = 1.201 \left(\frac{P}{29.92} \right) \left(\frac{530}{T} \right) \text{ (kg/m}^3\text{)}$$

where:

Re is the Reynolds number, defined as $\rho Dv/\mu$;

D is the pipe diameter;

ϵ is the dimension of irregularities in the conduit surface

f is the Fanning friction factor for conduit flow;

dP is the pressure difference along the conduit;

ρ is the density of the fluid;

μ is the viscosity of the fluid;

L is the conduit length;

- v is the average fluid velocity;
 K_T is the total of the applicable fitting coefficients in table 1;
 T is the air temperature in degrees ranking.
 P is the air pressure in inches of mercury.

Table 1
 Fitting Coefficients

Fitting	K
90° elbow	0.4-0.9
Standard 45° elbow	0.35-0.42
Tee, through side outlet	1.5
Tee, straight through	.4
180° bend	1.6
Entrance to circular pipe	0.25-0.50
Sudden expansion	$(1 - A_{up}/A_{dn})^2*$
Acceleration from $v = 0$ to $v = V_{entrance}$	1.0

Remarks:

For rectangular ducts, use the duct conversion program of this solution book.

This program assumes incompressible flow, thus accuracy will degenerate as velocity increases above 12,000 feet per minute.

No algorithm gives reliable outputs for transition flow ($2300 < Re < 4000$). If this condition is encountered, the program will halt displaying "TRANSITION". You may press [R/S] and the program will continue to an answer but the answer may have little or no relation to reality.

References:

Welty, Wicks, Wilson; *Fundamentals of Momentum, Heat and Mass Transfer*, John Wiley and Sons, Inc., 1969.

Baumeister, *Mark's Standard Handbook For Mechanical Engineers*, Seventh Edition, McGraw-Hill, 1967, p. 12-136.

* A_{up} is the upstream area and A_{dn} is the downstream area.

Example 1:

What pressure drop will force 6000 cubic feet per minute of 70°F air through 100 feet of 20 inch straight conduit. The atmospheric pressure is 29 inches of mercury.

Keystrokes: (SIZE \geq 018)	Display:
[///] [FIX]	
[XEQ] [ALPHA] AIRDUCT [ALPHA]	T,F=?
70 [R/S]	INHG=?
29 [R/S]	L,FT=?
100 [R/S]	Σ K=?
0 [R/S]	D,IN=?
20 [R/S]	SELECT KEY: dP V Q
[C]	Q,CFM=?
6000 [R/S]	INH20=0.41
[R/S]*	V,FPM=2750.73
[R/S]*	D,IN=?

* Press [R/S] if you are not using a printer.

Example 2:

The flow rate in Example 1 is to be increased to 15,000 cubic feet per minute by increasing the conduit diameter. What diameter is necessary?

Keystrokes:	Display:
30 [R/S]	SELECT KEY: dP V Q
[A]	INH20=?
[R/S]	V,FPM=3,551.69
[R/S]*	Q,CFM=17,430.93
[R/S]*	D,IN=?

The 30 inch duct will be adequate but try a 28 inch duct.

28 [R/S]	SELECT KEY: dP V Q
[A] [R/S]	V,FPM=3,401.48
[R/S]*	Q,CRM=14,542.07
[R/S]*	D,IN=?

Since duct is available only in even size use 30 inch duct.

User Instructions

				SIZE: 018
STEP	INSTRUCTIONS	INPUT	FUNCTION	DISPLAY
1.	Load program			
2.	Initialize program		[XEQ] AIRDUCT	T,F=?
3.	Key in air temperature in degrees Fahrenheit.	T	[R/S]	INHG=?
4.	Key in average atmospheric pressure in inches of mercury.	P _{atm}	[R/S]	L,FT=?
5.	Key in length of duct in feet	L	[R/S]	ΣK
6.	Key in sum of fitting coefficients from Table 1.	ΣK	[R/S]	D,IN=?
7.	Key in duct diameter in inches	D	[R/S]	SELECT KEY: dP V Q
8.	If you know pressure difference, press [A]		[A]	INH20=?
	If you know velocity, press [B]		[B]	V,FPM=?
	If you know volumetric flow rate press [C]		[C]	Q, CFM=?
9.	Key in known selected in step 8 and calculate remaining unknowns.	known	[R/S]	UNKNOWN ₁
			[R/S]*	UNKNOWN ₂
			[R/S]*	D,IN=?
10.	For a new diameter, or step 8 input, go to step 7. For a new case go to step 2. In either case, key in only values which change.			
*	Press [R/S] if you are not using a printer.			

Program Listings

<pre> 01♦LBL "AIR DUCT" 02 ADV 03 0 04 STO 00 05 "T,F" 06 XEQ "IN" 07 "INHG" 08 XEQ "IN" 09 RCL 01 10 460 11 + 12 STO 10 13 RCL X 14 1.5 15 Y↑X 16 1.101 E- 6 17 * 18 RCL Y 19 200 20 + 21 / 22 STO 16 23 RCL 02 24 29.92 25 / 26 530 27 RCL 10 28 / 29 * 30 1.201 31 * 32 STO 17 33 762 E-7 34 STO 03 35 3 36 STO 00 37 "L,FT" 38 .3048 39 ST/ 04 40 XEQ "IN" 41 .3048 42 ST* 04 43 1 44 ST+ 00 45 "ΣK" 46 XEQ "IN" 47♦LBL 15 48 4 49 STO 00 </pre>	<p>Calculate and store viscosity, density and surface irregularities.</p>	<pre> 50 "D, IN" 51 .0254 52 ST/ 05 53 XEQ "IN" 54 .0254 55 ST* 05 56 SF 27 57 "SELECT KEY:" 58 CF 21 59 AVIEW 60 SF 21 61 PSE 62♦LBL 01 63 "dP V Q" 64 PROMPT 65 GTO 01 66♦LBL A 67 6 68 STO 00 69 248.8 70 ST/ 07 71 "INH20" 72 XEQ "IN" 73 248.8 74 ST* 07 75 SF 03 76 XEQ 09 77♦LBL 03 78 RND 79 STO 15 80 XEQ 08 81 RND 82 RCL 15 83 X<>Y 84 X*Y? 85 GTO 03 86 XEQ "Re" 87 "V,FPM" 88 RCL 08 89 196.9 90 * 91 GTO 00 92♦LBL C 93 7 94 STO 00 95 "Q,CFM" 96 XEQ 11 97 * 98 * 99 STO 08 </pre>	<p>Input D.</p>
	<p>Input L.</p>		<p>Define keys.</p>
	<p>Input sum of fitting coefficients.</p>		<p>Input pressure difference.</p>
			<p>Compute velocity.</p>
			<p>Input flow rate.</p>

Program Listings

```

100 XEQ "IN"
101 XEQ 11
102 *
103 /
104 STO 08
105 XEQ 10
106 XEQ "Re"
107 "INH20"
108 RCL 07
109 248.8
110 /
111 XEQ "0"
112 "V,FPM"
113 RCL 08
114 196.9
115 *
116 XEQ "0"
117 ADV
118 GTO 15
119♦LBL B
120 7
121 STO 00
122 "V,FPM"
123 5.08 E-3
124 ST/ 08
125 XEQ "IN"
126 5.08 E-3
127 ST* 08
128 XEQ 10
129 XEQ "Re"
130 "INH20"
131 RCL 07
132 248.8
133 /
134♦LBL 00
135 XEQ "0"
136 "Q,CFM"
137 XEQ 11
138 *
139 *
140 XEQ "0"
141 ADV
142 GTO 15
143♦LBL 10
144 CF 03
145 XEQ 09
146 RCL 08
147 X↑2
148 *
149 RCL 17
150 *

```

Calculate
pressure drop.

Input velocity.

Calculate
pressure drop.

Output routine.

Calculate
pressure drop.

```

151 STO 07
152 RTN
153♦LBL 09
154 ADV
155 RCL 16
156 RCL 17
157 /
158 STO 09
159 RCL 05
160 RCL 03
161 /
162 STO 10
163 LN
164 1.737
165 STO 11
166 *
167 2.28
168 +
169 STO 12
170 STO 13
171 FS? 03
172 GTO 07
173♦LBL 08
174 16
175 RCL 08
176 RCL 05
177 *
178 RCL 09
179 /
180 STO 14
181 2300
182 X<=Y?
183 GTO 02
184 RDN
185 /
186 SQRT
187 1/X
188 STO 13
189 GTO 07
190♦LBL 02
191 RCL 12
192 RCL 13
193 -
194 4.67
195 RCL 10
196 *
197 RCL 14
198 /
199 RCL 13
200 *
201 1

```

Guess $1/\sqrt{f}$.

Special case
for low velocity
flow.

Turbulent flow
friction factor.

Program Listings

202 +		252 2300	
203 STO 00		253 RCL 14	
204 LN		254 X<=Y?	
205 RCL 11		255 RTN	
206 *		256 4000	
207 -		257 X>Y?	
208 RCL 00		258 PROMPT	
209 1/X		259 RTN	
210 CHS		260♦LBL 11	Convert between velocity and volumetric flow rate.
211 1		261 RCL 08	
212 +		262 RCL 05	
213 RCL 11		263 X↑2	
214 *		264 PI	
215 RCL 13		265 *	
216 /		266 4	
217 1		267 /	
218 +		268 2119	
219 /		269 RTN	
220 ST+ 13		270♦LBL "IN"	Input routine.
221 RCL 13		271 CF 22	
222 /		272 1	
223 ABS		273 ST+ 00	
224 1 E-3		274 RCL IND	
225 X<=Y?		00	
226 GTO 02		275 "F="	
227♦LBL 07	Compute velocity.	276 ASTO Y	
228 RCL 13		277 "F?"	
229 1/X		278 CF 21	
230 X↑2		279 AVIEW	
231 RCL 04		280 SF 21	
232 *		281 CLA	
233 RCL 05		282 ARCL Y	
234 /		283 STOP	
235 RCL 06		284 STO IND	
236 4		00	
237 /		285 FS? 22	
238 +		286 FC? 55	
239 ST+ X		287 RTN	
240 RCL 07		288 ARCL X	
241 RCL 17		289 PRA	
242 /		290 RTN	
243 X<>Y		291♦LBL "O"	Output routine.
244 FC? 03		292 "F="	
245 RTN		293 ARCL X	
246 /		294 AVIEW	
247 SQRT			
248 STO 08			
249 RTN			
250♦LBL "Re"			
251 "TRANSIT ION"	Check for transition.		
		00	

REGISTERS, STATUS, FLAGS, ASSIGNMENTS

DATA REGISTERS			STATUS			
00	Data Pointer	50	SIZE <u>018</u> TOT. REG. <u>107</u> USER MODE ENG _____ FIX _____ SCI _____ ON <u>X</u> OFF _____ DEG _____ RAD _____ GRAD _____			
05	D	55	FLAGS			
	ΣK		#	INIT S/C	SET INDICATES	CLEAR INDICATES
	dP		3		V calculation	dP calculation
	V/Q		27		USER mode	
	μ/ρ					
10	D/ ϵ	60				
	1.737					
	1/ \sqrt{f}					
	1/ \sqrt{f}					
	Re					
15	V	65				
	μ					
	δ					
20		70				
25		75				
30		80				
35		85				
			ASSIGNMENTS			
			FUNCTION		KEY	
40		90				
45		95				

AIR DUCT CONVERSION

This program converts a round, metal, HVAC, air duct to an equivalent rectangular air duct. The inverse conversion is also provided.

Equations:

$$D = \frac{1.3 (ab)^{0.625}}{(a + b)^{0.25}}$$

where:

- a is the depth (or width) of a rectangular duct in inches.
- b is the width (or depth) of a rectangular duct in inches.
- D is the approximate diameter for an equivalent round duct.

Reference:

Wolfe, James M.; Air Duct Conversion; HP-67/97 Users' Library Program 03046D.
 Baumeister, Mark's Standard Handbook for Mechanical Engineers, Seventh Edition,
 McGraw Hill, 1967, p. 12-137

Example 1:

A duct measuring 15 inches by 8 inches is to be replaced with a round duct.
 What diameter duct is required?

Keystrokes: (SIZE \geq 003)

Display:

[///] [FIX] 2

[XEQ] [ALPHA] REC-RND [ALPHA]

a=?

15 [R/S]

b=?

8 [R/S]

D=12.00

[R/S]*

a=?

Example 2:

A duct sizing program computes a diameter of 30 inches for a duct. Clearances only allow 24 inches in the vertical direction. What horizontal dimension is necessary for a rectangular duct?

Keystrokes: (SIZE \geq 003)	Display:
[///] [FIX] 2	
[XEQ] [ALPHA] RND-REC [ALPHA]	D=?
30 [R/S]	a=?
24 [R/S]	b=32
[R/S]*	D=?

*Press [R/S] if you are not using a printer.

Program Listings

<pre> 01♦LBL "REC -RND" 02♦LBL 01 03 ADV 04 0 05 STO 00 06 "a" 07 XEQ "IN" 08 "b" 09 XEQ "IN" 10 ADV 11 RCL 01 12 * 13 .625 14 Y↑X 15 RCL 01 16 RCL 02 17 + 18 SQRT 19 SQRT 20 / 21 1.3 22 * 23 "D" 24 .5 25 + 26 INT 27 XEQ "0" 28 GTO 01 29♦LBL "RND -REC" 30♦LBL 02 31 ADV 32 0 33 STO 00 34 "D" 35 XEQ "IN" 36 "a" 37 XEQ "IN" 38 RCL 02 39 RCL 01 40 * 41 RCL 02 42 ST+ X 43 RCL 01 44 - 45 / 46 STO 00 47 ADV 48♦LBL 03 </pre>	<p>Input a and b.</p> <hr/> <p>Calculate D.</p> <hr/> <p>Input D and a.</p> <hr/> <p>Guess b based on wetted perimeter.</p>	<pre> 49 RCL 00 50 RCL 02 51 * 52 .625 53 Y↑X 54 1.3 55 * 56 RCL 00 57 RCL 02 58 + 59 SQRT 60 SQRT 61 RCL 01 62 * 63 - 64 RCL 00 65 -.375 66 Y↑X 67 RCL 02 68 .625 69 Y↑X 70 * 71 .8125 72 * 73 RCL 02 74 RCL 00 75 + 76 -.75 77 Y↑X 78 RCL 01 79 * 80 4 81 / 82 - 83 / 84 ST- 00 85 RCL 00 86 / 87 ABS 88 .25 89 X<=Y? 90 GTO 03 91 RCL 00 92 .5 93 + 94 INT 95 "b" 96 XEQ "0" 97 GTO 02 98♦LBL "IN" 99 CF 22 </pre>	<p>Iterate by Newton's method to find b.</p> <hr/> <p>Output b.</p> <hr/> <p>Input subroutine</p>
--	---	--	---

EQUATIONS OF STATE

(Requires one memory module)

This program provides both ideal gas and Redlich-Kwong equations of state. Given four of the five state variables, the fifth is calculated. For the Redlich-Kwong solution, the critical pressure and temperature of the gas must be known. They are not needed for ideal gas solutions.

Values of the Universal Gas Constants

Value of R	Units of R	Units of P	Units of V	Units of T
8.314	N-m/g mole-K	N/m ²	m ³ /g mole	K
83.14	cm ³ -bar/g mole-K	bar	cm ³ /g mole	K
82.05	cm ³ -atm/g mole-K	atm	cm ³ /g mole	K
0.7302	atm-ft ³ /lb mole-°R	atm	ft ³ /lb mole	°R
10.73	psi-ft ³ /lb mole-°R	psi	ft ³ /lb mole	°R
1545	psf-ft ³ /lb mole-°R	psf	ft ³ /lb mole	°R

Critical Temperatures and Pressures

Substance	T _c , K	T _c , °R	P _c , ATM
Ammonia	405.6	730.1	112.5
Argon	151	272	48.0
Carbon dioxide	304.2	547.6	72.9
Carbon monoxide	133	239	34.5
Chlorine	417	751	76.1
Helium	5.3	9.5	2.26
Hydrogen	33.3	59.9	12.8
Nitrogen	126.2	227.2	33.5
Oxygen	154.8	278.6	50.1
Water	647.3	1165.1	218.2
Dichlorodifluoromethane	384.7	692.5	39.6
Dichlorofluoromethane	451.7	813.1	51.0
Ethane	305.5	549.9	48.2
Ethanol	516.3	929.3	63
Methanol	513.2	923.8	78.5
n-Butane	425.2	765.4	37.5
n-Haxane	507.9	914.2	29.9
n-Pentane	469.5	845.1	33.3
n-Octane	568.6	1023.5	24.6
Trichlorofluoromethane	471.2	848.1	43.2

Equations:

Ideal gas: $PV = nRT$

Redlich-Kwong:
$$P = \frac{nRT}{(V - b)} - \frac{a}{T^{1/2} V (V + b)}$$

$$a = 4.934 b nRT_c^{1.5}$$

$$b = 0.0867 \frac{nRT_c}{P_c}$$

where:

- P is the absolute pressure;
- V is the volume;
- n is the number of moles present;
- R is the universal gas constant;
- T is the absolute temperature;
- T_c is the critical temperature;
- P_c is the critical pressure.

Remarks:

P, V, n and T must have units compatible with R.

At low temperatures or high pressures, the ideal gas law does not represent the behavior of real gases.

No equation of state is valid for all substances or over an infinite range of conditions. The Redlich-Kwong equation gives moderate to good accuracy for a variety of substances over a wide range of conditions. Results should be used with caution and tempered by experience.

Solutions for V, n, R and T, using the Redlich-Kwong equation, require an iterative technique. Newton's method is employed using the ideal gas law to generate the initial guess. Iteration time is generally a function of the amount of deviation from ideal gas behavior. For extreme cases, the routine may fail to converge entirely, resulting in "DATA ERROR".

Example 1:

0.63 g moles of air are enclosed in a 25,000 cm³ space at 1200 K. What is the pressure in bars? Assume ideal gas behavior.

Keystrokes:

[XEQ] [ALPHA] SIZE [ALPHA] 015

[XEQ] [ALPHA] ID [ALPHA]

0 [R/S]

25000 [R/S]

0.63 [R/S]

83.14 [R/S]

1200 [R/S]

Display:

P?

V?

N?

R?

T?

P=2.51

Example 2:

The specific volume of a gas in a container is 800 cm³/g mole. The temperature will reach 400 K. What will the pressure be, according to the Redlich-Kwong relation?

$$P_c = 48.2 \text{ atm}$$

$$T_c = 305.5 \text{ K}$$

$$R = 82.05 \text{ cm}^3 - \text{atm/g mole-K}$$

Keystrokes:

[XEQ] [ALPHA] RK [ALPHA]

305.5 [R/S]

48.2 [R/S]

0 [R/S]

800 [R/S]

1 [R/S]

82.05 [R/S]

400 [R/S]

Display:

TC?

PC?

P?

V?

N?

R?

T?

P=36.29

Program Listings

01*LBL "ID"	Initialization	50 FS? 02	----- Calculate unknown	
02 0		51 RTN		
03 SF 00		52 GTO IND		
04 GTO 00		10		
05*LBL "RK"		53*LBL 05		
06 1		54 "P="		
07 CF 00		55 GTO 00		
08 "TC?"		56*LBL 06		
09 PROMPT		57 "V="		
10 STO 13		58*LBL 00		
11 "PC?"		59 RCL 07		
12 PROMPT		60 RCL 08		
13 STO 14		61 *		
14*LBL 00		62 RCL 09		
15 SF 02		63 *		
16 CF 01		64 RCL 05		
17 FIX 2		65 RCL 06		
18 "P?"		66 *		
19 PROMPT		67 /		
20 5		68 STO IND		
21 XEQ 00		10		
22 "V?"		69 GTO 00		
23 PROMPT		70*LBL 07		
24 6		71 SF 01		
25 XEQ 00		72 "N="		
26 "N?"		73 GTO 01		
27 PROMPT		74*LBL 08		
28 7		75 SF 01		
29 XEQ 00		76 "R="		
30 "R?"		77 GTO 01		
31 PROMPT		78*LBL 09		
32 8		79 "T="		
33 XEQ 00		80 SF 01		
34 "T?"		81*LBL 01		
35 PROMPT		82 RCL 05		
36 CF 02		83 RCL 06		
37 9		84 *		
38*LBL 00		85 RCL 07		
39 CF 01		86 /		
40 STO 01		87 RCL 08		
41 RDN		88 /		
42 STO IND		89 RCL 09		
01		90 /		
43 X≠0?		91 STO IND		
44 GTO 01		10		
45 R↑		92*LBL 00		
46 STO 10		93 FS? 00		
47 1		94 GTO 10		
48 STO IND		95 XEQ 01		
01	96 GTO 00			
49*LBL 01	97*LBL 02			

Program Listings

98 FS? 01		145 *	
99 XEQ 01		146 X↑2	
100♦LBL 00	If ideal, display	147 /	
101 RCL 00		148 RCL 00	
102 RCL 09		149 RCL 09	
103 *		150 *	
104 RCL 06		151 RCL 04	
105 RCL 12	Calculate using	152 X↑2	
106 -	Redlich-Kwong	153 /	
107 STO 04	equations	154 -	
108 /		155 RTN	
109 RCL 11		156♦LBL 09	$\frac{\partial P}{\partial T}$
110 RCL 09		157 RCL 00	
111 SQRT		158 RCL 04	
112 /		159 /	
113 STO 02		160 RCL 02	
114 RCL 06		161 2	
115 /		162 /	
116 LASTX		163 RCL 09	
117 RCL 12		164 /	
118 +		165 RCL 06	
119 STO 03		166 /	
120 /		167 RCL 03	
121 -		168 /	
122 RCL 05		169 +	
123 -		170 RTN	
124 XEQ IND		171♦LBL 07	$\frac{\partial P}{\partial n}$ or $\frac{\partial P}{\partial R}$
10		172♦LBL 08	
125 /		173 RCL 09	
126 ST- IND		174 RCL 06	
10		175 *	
127 RCL IND		176 RCL 04	
10		177 X↑2	
128 /		178 /	
129 ABS		179 RCL 06	
130 1 E-4		180 ENTER↑	
131 X<=Y?		181 +	
132 GTO 02		182 RCL 12	
133 RCL IND		183 +	
10		184 RCL 00	
134 GTO 10		185 /	
135♦LBL 06		186 RCL 06	
136 RCL 06		187 /	
137 ENTER↑	$\frac{\partial P}{\partial V}$	188 RCL 03	
138 +		189 X↑2	
139 RCL 12		190 /	
140 +		191 RCL 02	
141 RCL 02		192 *	
142 *		193 -	
143 RCL 03		194 RCL 00	
144 RCL 06		195 *	

Program Listings

196 RCL IND		51	
10			
197 /			
198 RTN			
199♦LBL 05			
200 LASTX			
201 +			
202 STO 05			
203 GTO 10			
204♦LBL 01	-----		
205 RCL 07	Calculate a, b	60	
206 RCL 08			
207 *			
208 STO 00			
209 .0867			
210 RCL 14			
211 /			
212 X<>Y			
213 RCL 13			
214 *			
215 *		70	
216 STO 12			
217 LASTX			
218 *			
219 RCL 13			
220 SQRT			
221 *			
222 4.934			
223 *			
224 STO 11			
225 RTN		80	
226♦LBL 10	-----		
227 ARCL X	Display		
228 AVIEW			
229 STOP			
230 .END.			
40		90	
50		00	

BLACK BODY THERMAL RADIATION

(Requires one memory module)

Bodies with finite temperatures emit thermal radiation. The higher the absolute temperature, the more thermal radiation emitted. Bodies which emit the maximum possible amount of energy at every wavelength for a specified temperature are said to be black bodies. While black bodies do not actually exist in nature, many surfaces may be assumed to be black for engineering considerations.

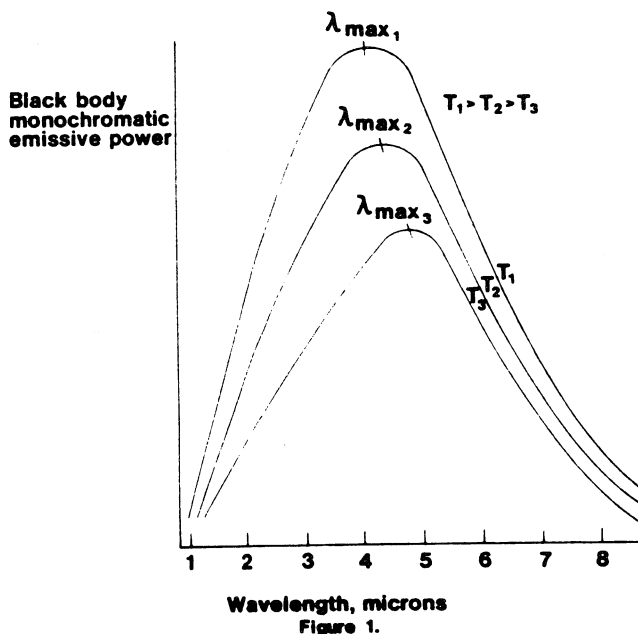


Figure 1.

Notes:

A half minute or more may be required to obtain $E_b(0-\lambda)$ or $E_b(\lambda_1-\lambda_2)$ since the integration is numerical.

Sources differ on values for constants. This could yield small discrepancies between published tables and program outputs.

Figure 1 is a representation of black body thermal emission as a function of wavelength. Note that as temperature increases, the area under the curves (total emissive power $E_b(0-\infty)$) increases. Also note that the wavelength of maximum emissive power λ_{max} shifts to the left as temperature increases.

This program calculates the wavelength of maximum emissive power for a given temperature, the temperature for which a given wavelength would be the wavelength of maximum emissive power, the total emissive power over all wavelengths, the emissive power at a particular wavelength, the emissive power from zero to a specified wavelength, and the emissive power between specified wavelengths.

Equations:

$$\lambda_{\max} T_{\lambda_{\max}} = c_3$$

$$E_{b(0-\infty)} = \sigma T^4$$

$$E_{b\lambda} = \frac{2\pi c_1}{\lambda^5 (e^{c_2/\lambda T} - 1)}$$

$$E_{b(0-\lambda)} = \int_0^\lambda E_{b\lambda} d\lambda$$

$$= 2\pi c_1 \sum_{k=1}^{\infty} -T/kc_2 e^{-\frac{kc_2}{T\lambda}} \left[\left(\frac{1}{\lambda} \right)^3 + \frac{3T}{\lambda^2 kc_2} + \frac{6}{\lambda} \left(\frac{T}{kc_2} \right)^2 + 6 \left(\frac{T}{kc_2} \right)^3 \right]$$

$$E_{b(\lambda_1 - \lambda_2)} = E_{b(0-\lambda_2)} - E_{b(0-\lambda_1)}$$

where:

λ_{\max} is the wavelength of maximum emissivity in microns;

T is the absolute temperature in $^{\circ}\text{R}$ or K ;

$E_{b(0-\infty)}$ is the total emissive power in Btu/hr-ft^2 or Watts/cm^2 ;

$E_{b\lambda}$ is the emissive power at λ in $\text{Btu/hr-ft}^2\text{-}\mu\text{m}$ or $\text{Watts/cm}^2\text{-}\mu\text{m}$;

$E_{b(0-\lambda)}$ is the emissive power for wavelengths less than λ in Btu/hr-ft^2 or Watts/cm^2 ;

$E_{b(\lambda_1 - \lambda_2)}$ is the emissive power for wavelengths between λ_1 and λ_2 in Btu/hr-ft^2 or Watts/cm^2 .

$$c_1 = 1.8887982 \times 10^7 \text{ Btu}\cdot\mu\text{m}^4/\text{hr}\cdot\text{ft}^2 \\ = 5.9544 \times 10^3 \text{ W}\mu\text{m}^4/\text{cm}^2$$

$$c_2 = 2.58984 \times 10^4 \mu\text{m}\cdot^{\circ}\text{R} = 1.4388 \times 10^4 \mu\text{m}\cdot\text{K}$$

$$c_3 = 5.216 \times 10^3 \mu\text{m}\cdot^{\circ}\text{R} = 2.8978 \times 10^3 \mu\text{m}\cdot\text{K}$$

$$\sigma = 1.713 \times 10^{-9} \text{ Btu/hr}\cdot\text{ft}^2\cdot^{\circ}\text{R}^4 = 5.6693 \times 10^{-12} \\ \text{W/cm}^2\cdot\text{K}^4$$

$$\sigma_{\text{exp}} = 1.731 \times 10^{-9} \text{ Btu/hr}\cdot\text{ft}^2\cdot^{\circ}\text{R}^4 = 5.729 \times 10^{-12} \\ \text{W/cm}^2\cdot\text{K}^4$$

References: HP-67/97 Users' Library Program.

Example:

What percentage of the radiant output of a lamp is in the visible range (0.4 to 0.7 microns) if the filament of the lamp is assumed to be a black body at 2400K?

Keystrokes: (SIZE \geq 009)

Display:

[USER]

(set USER mode)

[XEQ] [ALPHA] BB [ALPHA]

UNITS?

SI [R/S]

TEMP?

2400 [R/S]

WAVELENGTH?

.4 [R/S]

SOLVE

[F]

WV LNTH 2?

.7 [R/S]

EbL-L=4.9679

[C]

EbTOT=188.0938

[\div]

0.0264

100 [x]

2.6412

Program Listings

01*LBL "BB"	Initialize and prompt for units	47 RCL 06	Calculate T(λ_{max})
02 CLRG		48 /	
03 CF 22		49 "TEMP="	
04 "UNITS?"		50 ARCL X	
05 AON		51 PROMPT	
06 PROMPT		52*LBL C	Calculate E_b total
07 AOFF		53 RCL 05	
08 ASTO X		54 X \uparrow 2	
09 GTO IND		55 X \uparrow 2	
X		56 RCL 04	
10*LBL "SI"	Store units	57 *	
11 5954.4		58 "EbTOT="	
12 STO 01		59 ARCL X	
13 14388		60 PROMPT	
14 STO 02		61*LBL D	Calculate $E_{b\lambda}$
15 2897.8		62 RCL 01	
16 STO 03		63 ENTER \uparrow	
17 5.6693 E		64 +	
-12		65 PI	
18 STO 04		66 *	
19 GTO 00		67 RCL 06	
20*LBL "EN"		68 5	
21 18887982		69 Y \uparrow X	
22 STO 01		70 /	
23 25998.4		71 RCL 02	
24 STO 02		72 RCL 06	
25 5216		73 /	
26 STO 03		74 RCL 05	
27 .171312		75 /	
E-08		76 E \uparrow X	
28 STO 04		77 1	
29*LBL 00	Input prompting	78 -	
30 "TEMP?"		79 /	
31 PROMPT		80 "EbL="	
32 STO 05		81 ARCL X	
33 "WAVELEN		82 PROMPT	
GTH?"		83*LBL E	Calculate $E_b(0-\lambda)$
34 PROMPT		84 0	
35 STO 06		85 STO 08	
36 "SOLVE"		86 STO 07	
37 PROMPT		87*LBL 01	
38*LBL A	Calculate λ_{max}	88 RDN	
39 RCL 03		89 CLX	
40 RCL 05		90 RCL 08	
41 /		91 RCL 02	
42 "WL MAX="		92 RCL 05	
"		93 /	
43 ARCL X		94 -	
44 PROMPT		95 STO 08	
45*LBL B		96 3	
46 RCL 03		97 X<>Y	

Program Listings

98 /		149 "WV LNTH	
99 RCL 06		2?"	
100 X↑2		150 PROMPT	
101 /		151 ENTER↑	
102 LASTX		152 ENTER↑	
103 1/X		153 SF 00	
104 RCL 06		154 XEQ E	
105 /		155 X<>Y	
106 -		156 RCL 06	
107 6		157 STO 00	
108 RCL 06		158 RDN	
109 /		159 STO 06	
110 RCL 08		160 SF 00	
111 X↑2		161 XEQ E	
112 /		162 -	
113 -		163 ABS	
114 6		164 RCL 00	
115 RCL 08		165 STO 06	
116 X↑2		166 RDN	
117 /		167 "EbL-L="	
118 RCL 08		168 ARCL X	
119 /		169 PROMPT	
120 +		170 .END.	
121 RCL 08			
122 RCL 06			
123 /			
124 E↑X			
125 *			
126 RCL 08			
127 /			
128 ST+ 07		80	
129 RCL 07			
130 /			
131 1 E-05			
132 X<=Y?			
133 GTO 01			
134 RDN			
135 CLX			
136 RCL 07			
137 ENTER↑			
138 +		90	
139 PI			
140 *			
141 RCL 01			
142 *			
143 FS?C 00			
144 RTN			
145 "Eb0-L="			
146 ARCL X.			
147 PROMPT			
148♦LBL F	Calculate		
	$E_b(\lambda_1-\lambda_2)$	00	

PSYCHROMETRIC PROPERTIES

(Requires two memory modules)

Given pressure, drybulb temperature and either wet bulb temperature or relative humidity or vapor pressure, this program computes wet bulb temperature, dew point temperature, vapor pressure, humidity ratio, relative humidity, enthalpy and specific volume.

Either English or SI units may be used in problem solution.

Variable	English Units	SI Units
Temperature	°F	°C
Pressure	psi	kPa
Humidity Ratio	lb _m /lb _m dry air	kg/kg dry air
Relative Humidity	%	%
Enthalpy	Btu/lb _m dry air	kJ/kg dry air
Specific Volume	ft ³ /lb _m dry air	dm ³ /kg dry air

Temperatures may range from -40°F (-40°C) to 300 °F (150°C). For temperatures less than the ice point, vapor is assumed in equilibrium with ice.

Total pressure may range from 1.0 psi (7.0 kPa) to 50.0 psi (345.0 kPa).

Relative humidity may range between 0.0 and 100%.

Specific humidity must be less than 0.2.

If limits are exceeded program will halt with alpha diagnostic in Display.

Equations:

$$W = \frac{c_{p,a}(t_{wb} - t_{db}) + \omega_{sat,wb}(h_{g,wb} - h_{f,wb})}{h_{v,db} - h_{f,wb}}$$

$$c_{p,a} = 0.240 \text{ Btu/lb}_m \text{ } ^\circ\text{F} = 1.0048 \text{ kJ/kg } ^\circ\text{C}$$

$$h_v = h_g = a + bt$$

$$a = 1061.0 \text{ Btu/lb}_m = 2501.0 \text{ kJ/kg}$$

$$b = 0.445 \text{ Btu/lb}_m \text{ } ^\circ\text{F} = 1.8631 \text{ kJ/kg } ^\circ\text{C}$$

IF $t \geq 32^\circ\text{F}$ or 0°C

THEN $h_f = (t - c)d$

$$c = 32^\circ\text{F} = 0^\circ\text{C}$$

$$d = 1\text{Btu/lb}_m \text{ } ^\circ\text{F} = 4.1868 \text{ kJ/kg } ^\circ\text{C}$$

IF $t \geq 32^\circ\text{F}$ or 0°C THEN $h_f = h_i = [(t-c)0.467 + e]d$
 $e = -143.956^\circ\text{F} = -79.97556^\circ\text{C}$

$$H = c_{p,a} t_{db} + W h_{v,db}$$

$$W = \frac{R_{air}}{R_{vapor}} = \frac{PV}{P - PV} = \frac{R_{air}}{R_{vapor}} = 0.622$$

(also used to calculate P_{vapor})

$$P_{sat} = f e^{g/(t+h)}$$

t = temperature, $^\circ\text{F}$ or $^\circ\text{C}$

$$e = 2.718282$$

IF $t \geq 32^\circ\text{F}$ or 0°C THEN $f = 2.04466 \cdot 10^6$ psi = $1.40974 \cdot 10^7$ kPa
 $g = -7071.3^\circ\text{F} = -3928.5^\circ\text{C}$
 $h = 385^\circ\text{F} = 231.667^\circ\text{C}$

IF $t \geq 32^\circ\text{F}$ or 0°C THEN $f = 5.24506 \cdot 10^8$ psi = $3.61633 \cdot 10^9$ kPa
 $g = -11071^\circ\text{F} = -6150.6^\circ\text{C}$
 $h = 460^\circ\text{F} = 273.33^\circ\text{C}$

$$V = \frac{R_{air} T}{P_{total} - P_{vapor}}$$

$$REL = P_{vapor}/P_{sat,db}$$

where:

- P is the total pressure.
- PV is the vapor pressure
- t_{db} is the dry bulb temperature.
- P_{sat} is the saturation pressure.
- t_{wb} is the wet bulb temperature.
- t_{dp} is the dew point temperature.
- W is the humidity ratio.
- REL is the relative humidity.
- h is the enthalpy.
- V is the specific volume.

Reference:

HP-67 Users' Library Program 867D, Psychrometric Properties, Donald H. Madsen.

Example 1:

$P = 101.325 \text{ kPa}$, $T_{wb} = 20^\circ\text{C}$ $T_{db} = 25^\circ$

Keystrokes: (SIZE \geq 010)

Display:

[///] [FIX] 4

[XEQ] [ALPHA] PSYCHSI [ALPHA]

P=?

101.325 [R/S]

Tdb=?

25 [R/S]

PSAT=3.1762

[R/S]*

SELECT KEY: TWb REL PV

[A]

TWb=?

20 [R/S]

TdP=17.6023

[R/S]*

PV=2.0166

[R/S]*

W=0.0126

[R/S]*

REL=63.4931

[R/S]*

H=57.2983

[R/S]*

V=860.7494

[R/S]*

P=?

*Press [R/S] if you are not using a printer.

Example 2:

$P = 25 \text{ psi}$, $Tdb = 70.0^\circ\text{F}$, $PV = 0.182 \text{ psi}$

Keystrokes:

Display:

[///] [FIX] 4

[XEQ] [ALPHA] PSYCHE [ALPHA]

P=?

25 [R/S]

Tdb=?

70 [R/S]

PSAT=0.3640

[R/S]*

SELECT KEY: TWb REL PV

[E]

PV=?

.182 [R/S]

TWb=60.8398

[R/S]*

TdP=50.5726

[R/S]*

PV=0.1820

[R/S]*

W=0.0046

[R/S]*

REL=49.9988

[R/S]*

H=21.7817

[R/S]*

V=7.8987

[R/S]*

P=?

*Press [R/S] if you are not using a printer.

User Instructions

				SIZE: 010
STEP	INSTRUCTIONS	INPUT	FUNCTION	DISPLAY
1.	Load program			
2.	Initialize program for English units, or		[XEQ] PSYCHE	
	SI units.		[XEQ] PSYCHSI	P=?
3.	Key in total pressure.	P	[R/S]	Tdb=?
4.	Key in dry bulb temperature.	Tdb	[R/S]	PSAT=
			[R/S]*	SELECT KEY:
				TWb REL PV
5.	Press [A] if you know wet bulb temperature,		[A]	TWb=?
	[C] if you know relative humidity, or [E]		[B]	REL=?
	if you know vapor pressure, then go to		[C]	PV=?
	6a, 6b, or 6c.			
6a.	Key in wet bulb temperature and start			
	calculation.	TWb	[R/S]	
6b.	Key in relative humidity and start			
	calculation.	REL	[R/S]	TWb=
6c.	Key in vapor pressure and start calculation	PV	[R/S]	TWb=
7.	See outputs of:			
	Dew Point temperature,		[R/S]*	TdP=
	Vapor Pressure,		[R/S]*	PV=
	Humidity Ratio,		[R/S]*	W=
	Relative Humidity,		[R/S]*	REL=
	Enthalpy,		[R/S]*	H=
	Specific Volume		[R/S]*	V=
			[R/S]*	P=?
8.	For a new case using the same units, go to			
	step 3. Key in only values which change.			
*	Press [R/S] if you are not using a printer			

Program Listings

<pre> 01♦LBL "PSY CHSI" 02 SF 00 03 GTO 00 04♦LBL "PSY CHE" 05 CF 00 06♦LBL 00 07 0 08 STO 00 09 ADV 10 "P" 11 XEQ "IN" 12 "Tdb" 13 XEQ "IN" 14 XEQ F 15 ADV 16 "PSAT" 17 XEQ "0" 18 STO 06 19 ADV 20 "SELECT KEY:" 21 CF 21 22 AVIEW 23 SF 21 24 PSE 25♦LBL 22 26 SF 27 27 "TWb RE L PV" 28 PROMPT 29 GTO 22 30♦LBL A 31 2 32 STO 00 33 "TWb" 34 XEQ "IN" 35 XEQ F 36 XEQ 03 37 "TWb HIG H" 38 X<0? 39 PROMPT 40 XEQ 04 41 "TWb LOW " 42 X<0? 43 PROMPT 44 STO 07 45 .2 </pre>	Initialize for SI units.	<pre> 46 "SPC HUM >=.2" 47 X<=Y? 48 PROMPT 49 RDN 50 RCL 01 51 * 52 RCL 07 53 .622 54 + 55 / 56 "TWb>Tdb " 57 XEQ 05 58 ADV 59 GTO 18 60♦LBL C 61 3 62 STO 00 63 "REL" 64 XEQ "IN" 65 ADV 66 RCL 02 67 STO 03 68 XEQ F 69 X<>Y 70 % 71 STO 08 72 GTO 00 73♦LBL E 74 RCL 02 75 STO 03 76 7 77 STO 00 78 "PV" 79 XEQ "IN" 80 "VP>Tdb" 81 ADV 82 XEQ 05 83 RCL 08 84♦LBL 00 85 XEQ 03 86 "VP>P" 87 X<0? 88 PROMPT 89 STO 07 90 .2 91 "W>.2" 92 X<=Y? 93 PROMPT 94 FS? 00 </pre>	Input relative humidity.
	Initialize for English units.		
	Input T and T _{db} .		
	Calculate P _{sat} .		
	Prompt user to select key [A], [C], or [E].		
	Input T _{wb} .		Input vapor pressure.

Program Listings

```

95 80
96 FC? 00
97 140
98 STO 09
99 CF 02
100♦LBL 01
101 RCL 09
102 FS?C 02
103 CHS
104 ST- 03
105 2
106 ST/ 09
107 RCL 03
108 XEQ F
109 XEQ 03
110 X<0?
111 GTO 01
112 XEQ 04
113 RCL 07
114 -
115 X<0?
116 SF 02
117 ABS
118 1 E-5
119 X<=Y?
120 GTO 01
121 GTO 08
122♦LBL 06
123 FC? 00
124 .445
125 FS? 00
126 1.8631
127 *
128 FC? 00
129 1061
130 FS? 00
131 2501
132 +
133 X<>Y
134 32
135 FS? 00
136 CLX
137 -
138 X<0?
139 XEQ 07
140 FC? 00
141 1
142 FS? 00
143 4.1868
144 *
145 -

```

Calculate T_{wb} .

Calculate
enthalpy
difference.

```

146 RTN
147♦LBL 07
148 .467
149 *
150 FC? 00
151 -143.956
152 FS? 00
153 -79.9755
6
154 +
155 RTN
156♦LBL 05
157 STO 08
158 RCL 06
159 /
160 1
161 X<>Y
162 X>Y?
163 PROMPT
164 1 E2
165 *
166 STO 04
167 RTN
168♦LBL 08
169 RCL 03
170 "TWb"
171 XEQ "0"
172♦LBL 18
173 RCL 08
174 X=0?
175 GTO 09
176 32
177 FS? 00
178 CLX
179 XEQ F
180 X>Y?
181 GTO 00
182 RCL 08
183 FS? 00
184 1.40974
E7
185 FC? 00
186 2.04466
E6
187 /
188 LN
189 1/X
190 FS? 00
191 -3928.5
192 FC? 00
193 -7071.3

```

Relative
humidity
calculation.

Print results.

Program Listings

<pre> 194 * 195 FS? 00 196 231.667 197 FC? 00 198 385 199 - 200 GTO 11 201*LBL 00 202 RCL 08 203 FS? 00 204 3.61633 E9 205 FC? 00 206 5.24506 E8 207 / 208 LN 209 1/X 210 FS? 00 211 -6150.6 212 FC? 00 213 -11071 214 * 215 FS? 00 216 273.33 217 FC? 00 218 460 219 - 220 GTO 11 221*LBL F 222 32 223 FS? 00 224 CLX 225 X>Y? 226 GTO 00 227 RDN 228 FS? 00 229 231.667 230 FC? 00 231 385 232 + 233 FS? 00 234 -3928.5 235 FC? 00 236 -7071.3 237 X<>Y 238 / 239 E↑X 240 FS? 00 241 1.40974 E7 242 FC? 00 </pre>		<pre> 243 2.04466 E6 244 * 245 RTN 246*LBL 00 247 RDN 248 FS? 00 249 273.33 250 FC? 00 251 460 252 + 253 FS? 00 254 -6150.6 255 FC? 00 256 -11071 257 X<>Y 258 / 259 E↑X 260 FS? 00 261 3.61633 E9 262 FC? 00 263 5.24506 E8 264 * 265 RTN 266*LBL 03 267 "WSAT OR VP=P" 268 .622 269 X<>Y 270 * 271 RCL 01 272 LASTX 273 - 274 X=0? 275 PROMPT 276 / 277 RTN 278*LBL 04 279 RCL 03 280 RCL 03 281 XEQ 06 282 * 283 RCL 03 284 RCL 02 285 - 286 FC? 00 287 .24 288 FS? 00 289 1.0048 </pre>	<p>Saturation pressure for sub-icepoint conditions.</p>
	<p>Saturation pressure subroutine.</p>		<p>Calculate specific humidity from vapor pressure.</p>
			<p>Calculate specific humidity from wet and dry bulb temperatures.</p>

Program Listings

290 *		341 "V"	
291 +		342 XEQ "0"	
292 RCL 03		343 GTO 00	
293 RCL 02		344♦LBL "IN"	Input subroutine.
294 XEQ 06		345 CF 22	
295 /		346 1	
296 RTN		347 ST+ 00	
297♦LBL 11	Output values.	348 RCL IND	
298 "TdP"		00	
299 XEQ "0"		349 "f="	
300♦LBL 09		350 ASTO Y	
301 RCL 08		351 "f?"	
302 "PV"		352 CF 21	
303 XEQ "0"		353 AVIEW	
304 RCL 07		354 SF 21	
305 "W"		355 CLA	
306 XEQ "0"		356 ARCL Y	
307 RCL 04		357 STOP	
308 "REL"		358 STO IND	
309 XEQ "0"		00	
310 RCL 02		359 FS? 22	
311 FC? 00		360 FC? 55	
312 .24		361 RTN	
313 FS? 00		362 ARCL X	
314 1.0048		363 PRA	
315 *		364 RTN	
316 32		365♦LBL "0"	Output subroutine
317 FS? 00		366 "f="	
318 ST- X		367 ARCL X	
319 RCL 02		368 AVIEW	
320 XEQ 06			
321 RCL 07			
322 *			
323 +			
324 "H"			
325 XEQ "0"			
326 RCL 02			
327 FC? 00			
328 459.67			
329 FS? 00			
330 273.15		90	
331 +			
332 FC? 00			
333 .3701			
334 FS? 00			
335 286.7			
336 *			
337 RCL 01			
338 RCL 08			
339 -			
340 /		00	

HEAT EXCHANGERS

(Requires one memory module)

This program allows analysis of counterflow, parallel flow, parallel-counterflow, and crossflow heat exchangers.

Figure 1:

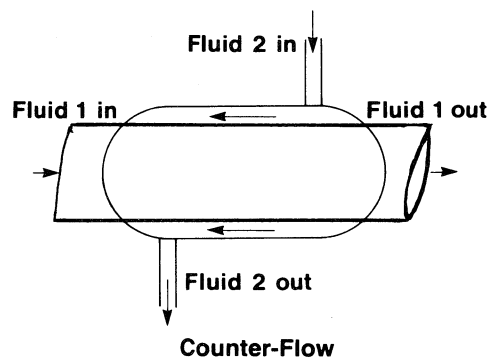


Figure 2:

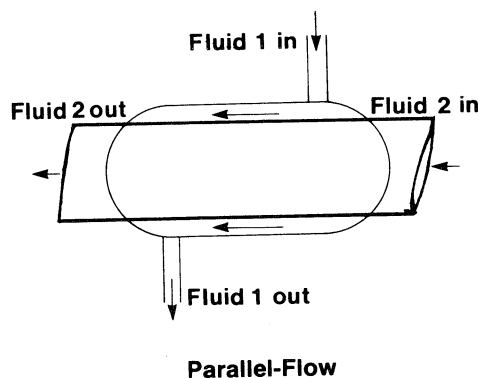


Figure 3:

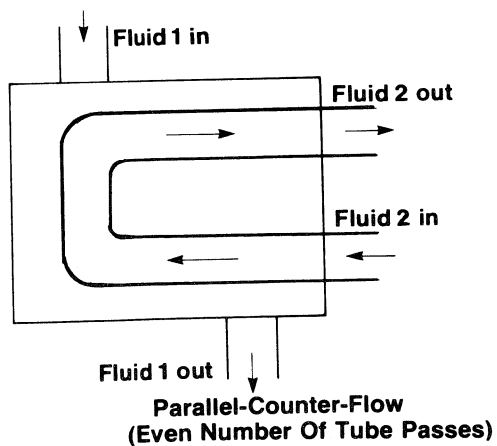
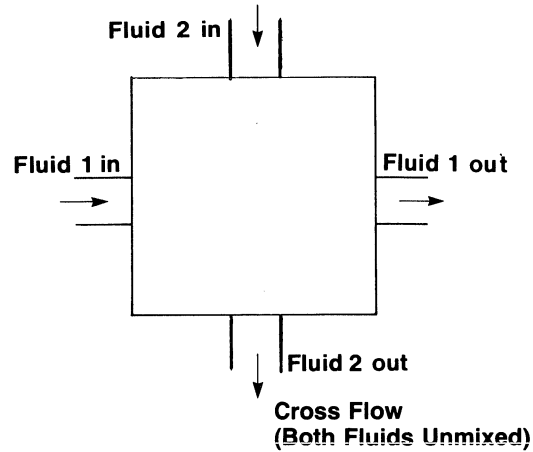


Figure 4:



Equations:

Heat exchanger effectiveness E is the ratio of actual heat transfer to maximum possible heat transfer.

$$E = \frac{Q}{C_{\min} (T_{hin} - T_{cin})} = \frac{C_h (T_{hin} - T_{ho})}{C_{\min} (T_{hin} - T_{cin})} = \frac{C_c (T_{co} - T_{cin})}{C_{\min} (T_{hin} - T_{cin})}$$

where:

Q is the actual heat transfer.

T_{hin} and T_{cin} are the inlet temperatures of the hot and cold fluids respectively.

T_{ho} and T_{co} are the outlet temperatures of the hot and cold fluids respectively.

C_h and C_c are the heat capacities of the hot and cold fluids, respectively, e.g., $C_h = m_h \times c_{ph}$, where m_h is the flow rate and c_{ph} is the specific heat capacity of the hot fluid.

C_{\min} and C_{\max} (which are used later) are the smaller and larger values of C_h and C_c .

Effectiveness can be related to the product of the surface area of the heat exchanger and the overall heat transfer coefficient for specific geometries. This product is designated AU. The geometries considered in this paper have the following correlations:

Counterflow (see figure 1)

$$E = \frac{1 - e^{-\frac{AU}{C_{\min}} \left(1 - \frac{C_{\min}}{C_{\max}}\right)}}{1 - \left(\frac{C_{\min}}{C_{\max}}\right) e^{-\frac{AU}{C_{\min}} \left(1 - \frac{C_{\min}}{C_{\max}}\right)}}$$

For $C_{\min}/C_{\max} = 1$

$$E = \frac{AU/C_{\min}}{1 + AU/C_{\min}}$$

Parallel Flow (see figure 2)

$$E = \frac{1 - e^{-\frac{AU}{C_{\min}} (1 + C_{\min}/C_{\max})}}{1 + C_{\min}/C_{\max}}$$

For $C_{\min}/C_{\max} = 0$, C_{\min} is set to 1.

Parallel-Counterflow (well mixed with an even number of tube passes; see Figure 3)

$$E = \frac{2}{\left(1 + \frac{C_{\min}}{C_{\max}}\right) + \sqrt{1 + \left(\frac{C_{\min}}{C_{\max}}\right)^2} \left[\frac{1 + e^{-x}}{1 - e^{-x}}\right]}$$

where:

$$x = \frac{AU}{C_{\min}} \sqrt{1 + \left(\frac{C_{\min}}{C_{\max}}\right)^2}$$

Crossflow (both fluids unmixed; see figure 4)

No exact expression exists for this case, but the following is a very good approximation. Note that an iterative solution is required for AU.

$$E = 1 - e \left(e \left(-\frac{AU}{C_{\min}} \frac{C_{\min}}{C_{\max}} y \right) - 1 \right) \left(\frac{C_{\max}}{C_{\min}} \frac{1}{y} \right)$$

where:

$$y = \left[\frac{C_{\min}}{AU} \right]^{0.22}$$

References:

W.M. Kays and A.L. London, *Compact Heat Exchangers*, National Press, 1955
 Eckert and Drake, *Heat and Mass Transfer*, McGraw-Hill.

Remarks:

For cases where the inlet and outlet temperatures of one of the fluids are equal (change of phase), use zero for the heat capacity of that fluid.

The solution for AU in the crossflow configuration takes significantly longer than other solutions because of the iterative technique required.

The program must be allowed to solve for all values (AU, Q, T_{co} , T_{ho} , and E). It is quite possible for the heat balance equations to yield physically meaningless solutions for a particular configuration. However, the message "2ND LAW ERR" will be displayed if the 2nd law of thermodynamics has been violated during the calculation of AU or Q.

This program is organized into five routines. The first routine performs heat balance calculations and acts as a controller for the four configuration subroutines. Each configuration subroutine has two sections that calculate AU and E for that heat exchanger. You should first load the controller, then load the configuration of interest as a separate program.

You may wish to write your own configuration routines. A routine for a configuration must be in the following format:


```

LBL ACON
.
.
.
(calculates AU for this configuration)
.
.
.
RTN
.
.
.
LBL ECON
.
.
.
(calculates E for this configuration)
.
.
.
END

```

Example:

A liquid at 168°F is to be cooled to 117°F. The liquid has a heat capacity of 0.42 Btu/LBM-°F and flows at 7700 LBM/hr. Cooling water (heat capacity = 1.00) is available at 4800 lbm/hr at 50°F. For counterflow, crossflow, parallel-counterflow, and parallel flow heat exchangers with overall coefficients of 55 Btu/hr-ft²-°F what areas are required?

Keystrokes: (SIZE ≥ 023)

Display:

[///] [FIX] 4

Load main routine and counterflow subroutine.

[XEQ] [ALPHA] HEATX [ALPHA]

TC IN=?

50 [R/S]

TH IN=?

168 [R/S]

MC=?

4800 [R/S]

MH=?

7700 [R/S]

GPC=?

1 [R/S]

CPH=?

.42 [R/S]

SELECT KEY: E AU Q TC TH

Since the temperature of the outgoing fluid is known, press the [E] key.

[E]

THO=?

117 [R/S]

E=0.4322

[R/S]*

AU=2,198.7662

[R/S]*

Q=164,933.9999

[R/S]*

TCO=84.3612

[R/S]*

SELECT KEY: E AU Q TC TH

Keystrokes:	Display:
Since $A = AU/U$, calculate A.	
2198.7662 [ENTER] 55 [÷]	39.9776
Load crossflow subroutine.	
[XEQ] [ALPHA] HEATX [ALPHA]	TC IN=?
[R/S]	TH IN=?
[R/S]	MC=?
[R/S]	MH=?
[R/S]	CPC=?
[R/S]	CPH=?
[R/S]	SELECT KEY: E AU Q TC TH
[E]	THO=?
[R/S]	E=0.4322
[R/S]*	AU=2,353.6675
[R/S]*	Q=164,934.0000
[R/S]*	TCO=84.3613
[R/S]	SELECT KEY: E AU Q TC TH
2353.6675 [ENTER] 55 [÷]	42.7940

An analogous procedure will yield areas of 42.2776 ft^2 and 45.1494 ft^2 for parallel-counterflow and parallel exchanges respectively.

User Instructions

				SIZE: 023
STEP	INSTRUCTIONS	INPUT	FUNCTION	DISPLAY
1.	Load program and then:		[GTO] ..	
2.	Load configuration subroutine corresponding			
	to your heat exchanger geometry		[XEQ] HEATX	TC IN=?
3.	Input inlet temperature of cold fluid	T_{cin}	[R/S]	TH IN=?
4.	Input inlet temperature of hot fluid	T_{hin}	[R/S]	MC=?
5.	Input mass flow rate of cold fluid	m_c	[R/S]	MH=?
6.	Input mass flow rate of hot fluid	m_h	[R/S]	CPC=?
7.	Input specific heat of cold fluid	C_{pc}	[R/S]	CPH=?
8.	Input specific heat of hot fluid	C_{ph}	[R/S]	SELECT KEY
				E AU Q TC TH
9.	Select the known value:			
	heat exchanger effectiveness		[A]	E=?
	area-heat transfer coefficient product		[B]	AU=?
	heat transfer		[C]	Q=?
	outlet temperature of cold fluid		[D]	TCO=?
	outlet temperature of hot fluid		[E]	THO=?
	input the known value.	E	[R/S]	
		AU	[R/S]	
		Q	[R/S]	
		TCO	[R/S]	
		THO	[R/S]	
	The four variables other than the one you			E=
	input will be output. The output order		[R/S]*	AU=
	will vary depending on which value was		[R/S]*	Q=
	input. If the 2nd law of thermodynamics		[R/S]*	TCO=
	is violated, the message "2ND LAW ERR"		[R/S]*	THO=
	will be displayed.		[R/S]*	SELECT KEY

User Instructions

SIZE: 023

STEP	INSTRUCTIONS	INPUT	FUNCTION	DISPLAY
10.	For a new problem, go to step 2 or step 9.			E AU Q TC TH
	It is not necessary to key in any values			
	which do not change. Ignore the prompts			
	and press [R/S].			
*	Press [R/S] if you do not have a printer.			

Program Listings

Heat Exchanger - Main Routine

01*LBL "HEA TX"	Input values.	49 XEQ "IN"	
02 2		50 ADV	
03 STO 00		51 GTO 16	
04 "TC IN"		52*LBL B	Input AU.
05 XEQ "IN"		53 SF 03	
06 "TH IN"		54 10	
07 XEQ "IN"		55 STO 00	
08 14		56 "AU"	
09 STO 00		57 XEQ "IN"	
10 "MC"		58 ADV	
11 XEQ "IN"		59 GTO 01	
12 "MH"		60*LBL C	Input Q.
13 XEQ "IN"		61 SF 04	
14 "CPC"		62 11	
15 XEQ "IN"		63 STO 00	
16 RCL 15		64 "Q"	
17 *		65 XEQ "IN"	
18 STO 05		66 ADV	
19 "CPH"		67 GTO 05	
20 XEQ "IN"		68*LBL D	Input TCO.
21 RCL 16		69 SF 05	
22 *		70 12	
23 STO 06		71 STO 00	
24 "CON"		72 "TCO"	
25 ASTO 22		73 XEQ "IN"	
26*LBL 06		74 ADV	
27 CF 02		75 GTO 14	
28 CF 03	76*LBL E	Input THO.	
29 CF 04	77 SF 06		
30 CF 05	78 13		
31 CF 06	79 STO 00		
32 CF 21	80 "THO"		
33 SF 27	81 XEQ "IN"		
34 "SELECT	82 ADV		
KEY:"	83 GTO 04		
35 AVIEW	84*LBL 16	Calculate AU.	
36 SF 21	85 FS?C 03		
37 PSE	86 GTO 06		
38*LBL 00	87 RCL 10		
39 ADV	88 "A"		
40 "E AU Q	89 XEQ 08		
TC TH"	90 STO 11		
41 PROMPT	91 "AU"		
42 GTO 00	92 XEQ "O"		
43*LBL A	93*LBL 01	Calculate Q.	
44 SF 02	94 FS?C 04		
45 9	95 GTO 06		
46 STO 00	96 RCL 11		
47 SF 01	97 "E"		
48 "E"	98 XEQ 08		
	99 RCL 07		

Program Listings

Heat Exchanger - Main Routine

100 *		151 X<>Y	
101 RCL 04		152 RCL 04	
102 RCL 03		153 RCL 03	
103 -		154 -	
104 *		155 /	
105 STO 12		156 RCL 05	
106 "0"		157 RCL 06	
107 XEQ "0"		158 X<=Y?	
108*LBL 05		159 X<>Y	
109 FS?C 05		160 RDN	
110 GTO 06	Calculate TCO.	161 X=0?	
111 RCL 12		162 X<> T	
112 RCL 05		163 /	
113 X#0?		164 STO 10	
114 /		165 SF 01	
115 RCL 03		166 "E"	
116 +		167 XEQ "0"	
117 STO 13		168 GTO 16	
118 "TCO"		169*LBL "A0"	
119 XEQ "0"		170 1	
120*LBL 14		171 RCL 10	
121 FS?C 06		172 -	
122 GTO 06	Calculate THO.	173 LN	
123 RCL 13		174 CHS	A0 for $C_{min}=0.00$.
124 RCL 03		175 RTN	
125 -		176*LBL "E0"	
126 RCL 05		177 1	
127 *		178 RCL 11	
128 RCL 06		179 CHS	
129 X#0?		180 E↑X	E0 for $C_{min}=0.00$.
130 /		181 -	
131 RCL 04		182 RTN	
132 -		183*LBL 08	
133 CHS		184 RCL 05	
134 STO 14		185 RCL 06	
135 "THO"		186 X>Y?	
136 XEQ "0"		187 X<>Y	
137*LBL 04		188 X<>Y	
138 FS?C 02		189 STO 07	
139 GTO 06		190 X<>Y	
140 RCL 13	Calculate E.	191 X#0?	
141 RCL 03		192 STO 07	
142 -		193 X<>Y	
143 RCL 05		194 X#0?	
144 *		195 /	
145 RCL 04		196 STO 09	
146 RCL 14		197 SF 25	
147 -		198 X=0?	
148 RCL 06		199 "F0"	
149 *		200 X#0?	
150 X=0?		201 ARCL 22	Find C_{min} and execute configuration subroutine.

Program Listings

202	ASTO T		51	
203	XEQ IND			
	T			
204	FS?C 25			
205	RTN			
206	"2ND LAW			
	ERR"	Trap errors from		
207	PROMPT	subroutines		
208	GTO 06			
209	*LBL "IN"			
210	CF 22	Input subroutine	60	
211	1			
212	ST+ 00			
213	RCL IND			
	00			
214	"F="			
215	ASTO Y			
216	"F?"			
217	CF 21			
218	AVIEW			
219	SF 21		70	
220	CLA			
221	ARCL Y			
222	STOP			
223	STO IND			
	00			
224	FS? 22			
225	FC? 55			
226	RTN			
227	ARCL X			
228	PRA		80	
229	RTN	Print if printer		
230	*LBL "O"	is attached		
231	"F="			
232	ARCL X	Output subroutine		
233	AVIEW			
234	.END.			
40			90	
50			00	

Program Listings

Parallel Flow Subroutine

01	LBL "ACO	Calculate AU.	51	
N"				
02	RCL 09			
03	1			
04	+			
05	RCL 10			
06	*			
07	CHS			
08	1			
09	+			
10	LN		60	
11	CHS			
12	1			
13	RCL 09			
14	+			
15	/			
16	RCL 07			
17	*			
18	RTN			
19	LBL "ECO			
N"		Calculate E.	70	
20	1			
21	+			
22	RCL 11			
23	RCL 07			
24	/			
25	*			
26	CHS			
27	E↑X			
28	CHS			
29	1	80		
30	+			
31	1			
32	RCL 09			
33	+			
34	/			
35	RTN			
40			90	
50			00	

Program Listings

Counter Flow Subroutine

<pre> 01♦LBL "ACO N" 02 RCL 10 03 1/X 04 - 05 1 06 LASTX 07 - 08 / 09 LN 10 1 11 RCL 09 12 - 13 X=0? 14 GTO 10 15 / 16 RCL 07 17 * 18 RTN 19♦LBL 10 20 RCL 10 21 1 22 RCL 10 23 - 24 / 25 RCL 07 26 * 27 RTN </pre>	<p>Calculate AU.</p>	<pre> 50 RCL 11 51 RCL 07 52 / 53 ENTER↑ 54 ENTER↑ 55 1 56 + 57 / 58 RTN </pre>
<pre> 28♦LBL "ECO N" 29 1 30 - 31 RCL 11 32 RCL 07 33 / 34 * 35 E↑X 36 1 37 X<>Y 38 - 39 LASTX 40 RCL 09 41 * 42 1 43 X<>Y 44 - 45 X=0? 46 GTO 11 47 / 48 RTN 49♦LBL 11 </pre>	<p>Calculate E.</p>	

Program Listings

Parallel-Counter Flow Subroutine

01♦LBL "ACO N"	Calculate AU.	50♦LBL 12	
02 XEQ 12		51 RCL 09	
03 2		52 1	
04 *		53 +	
05 RCL 12		54 STO 08	
06 2		55 RCL 09	
07 RCL 10		56 X↑2	
08 /		57 1	
09 +		58 +	
10 RCL 08		59 SQRT	
11 -		60 STO 12	
12 /		61 RTN	
13 CHS			
14 1			
15 +			
16 LN			
17 RCL 12			
18 /			
19 CHS			
20 RCL 07		70	
21 /			
22 LASTX			
23 X↑2			
24 *			
25 RTN			
26♦LBL "ECO N"	Calculate E.		
27 XEQ 12			
28 RCL 11		80	
29 RCL 07			
30 /			
31 RCL 12			
32 *			
33 CHS			
34 E↑X			
35 1			
36 X<>Y			
37 +			
38 1			
39 LASTX		90	
40 -			
41 /			
42 RCL 12			
43 *			
44 RCL 08			
45 +			
46 2			
47 X<>Y			
48 /			
49 RTN		00	

Program Listings

Cross Flow Subroutine

01♦LBL "ACO		49 E↑X
N"	Calculate AU.	50 1
02 0		51 -
03 STO 19		52 *
04 1		53 E↑X
05 RCL 10		54 CHS
06 CHS		55 1
07 STO 21		56 +
08 +		
09 LN		60
10 CHS		
11 STO 11		
12♦LBL 13		
13 RCL 11		
14 XEQ "ECO		
N"		
15 RCL 10		
16 -		
17 STO 20		
18 RCL 19		70
19 RCL 11		
20 STO 19		
21 -		
22 RCL 21		
23 RCL 20		
24 STO 21		
25 -		
26 /		
27 *		
28 ST- 11		80
29 ABS		
30 1 E-4		
31 X<=Y?		
32 GTO 13		
33 RCL 11		
34 RTN		
35♦LBL "ECO		
N"	Calculate E.	
36 RCL 11		
37 RCL 07		90
38 /		
39 ENTER↑		
40 ENTER↑		
41 .22		
42 Y↑X		
43 RCL 09		
44 /		
45 /		
46 LASTX		
47 X<>Y		
48 CHS		00

REGISTERS, STATUS, FLAGS, ASSIGNMENTS

DATA REGISTERS			STATUS				
00	Storage Index	50	SIZE	23	TOT. REG.	102	USER MODE
			ENG		FIX		ON X OFF
			DEG		RAD		GRAD
	TC IN		FLAGS				
	TH IN						
05	CC	55	#	INIT S/C	SET INDICATES	CLEAR INDICATES	
	CH		0		Unit conversion		
	Cmin		1	C			
	Cmax		2	C			
	Cmin/Cmax		3	C			
10	E	60	4	C			
	AU		5	C			
	Q		6	C			
	Tco		23		Alpha input		
	Tho		55		Printer connected		
15	MC	65					
	MH						
	cpc						
	cph						
	(AU _{i-1})						
20	F(AU _i)	70					
	F(AU _{i-1})						
	"CON"						
25		75					
30		80					
35		85					
			ASSIGNMENTS				
			FUNCTION	KEY	FUNCTION	KEY	
40		90					
45		95					

DECIBEL ADDITION AND SUBTRACTION

This program adds or subtracts sound pressure levels measured in decibels.

Equations:

$$dB_1 + dB_2 = 10 \log (10^{dB_1/10} + 10^{dB_2/10})$$

$$dB_1 - dB_2 = 10 \log (10^{dB_1/10} - 10^{dB_2/10})$$

When subtracting, if $dB_1 < dB_2$, the program will exchange values.

Example 1:

A noise level of 72 decibels is measured in a room. The air conditioning is turned on and the noise level increases to 74 decibels. What is the noise level of the air conditioning system.

Keystrokes:

Display:

[///] [FIX] 2

74 [ENTER] 72 [XEQ] [ALPHA] dB- [ALPHA] 69.67 dB

Example 2:

A compressor is known to have a sound pressure level of 90 dB. The background is 85 dB. What is the total?

Keystrokes:

Display:

[///] [FIX] 2

90 [ENTER] 85 [XEQ] [ALPHA] dB+ [ALPHA] 91.19dB

Program Listings

01♦LBL "dB+	Add decibels.	51	
02 XEQ 00			
03 +			
04 GTO 01			
05♦LBL "dB-			
06 XEQ 00	Subtract decibels.		
07 -			
08 ABS	Display result.	60	
09♦LBL 01			
10 LOG			
11 10			
12 *			
13 CLA			
14 ARCL X			
15 "F dB"			
16 AVIEW			
17 RTN			
18♦LBL 00	Convert for add or subtract.	70	
19 10			
20 ST/ Z			
21 /			
22 X<>Y			
23 10↑X			
24 X<>Y			
25 10↑X			
30		80	
40		90	
50		00	

TEMPERATURE CONVERSION

This program converts interchangeably between the four types of temperature.

Equations:

$$K = (°F + 459.67)/1.8$$

$$K = °C + 273.15$$

$$K = °R / 1.8$$

where:

K is temperature in Kelvins.

°F is temperature in degrees Fahrenheit.

°C is temperature in degrees Celsius.

°R is temperature in degrees Rankine.

Remarks:

Only the stack registers, LASTx and the alpha register are used in the conversions.

Example:

Convert: 472K to °R
 27°F to °C
 25°C to °F
 100°C to °F

Keystrokes:

Display:

[///] [FIX] 2	
[XEQ] [ALPHA] TCON [ALPHA]	F C R K
472 [D]	F C R K
[C]	849.60 (°R)
[R/S]	F C R K
27 [A]	F C R K
[B]	-2.78 (°C)
25 [B]	F C R K
[A]	77 (°F)
100 [B]	F C R K
[A]	212 (°F)

Program Listings

01♦LBL 00	Display answer	51	
02 RTN			
03♦LBL "TCO N"	Initialize		
04 SF 27			
05 "F C R K"			
06 PROMPT			
07♦LBL A	°F-K	60	
08 459.67			
09 +			
10 1.8			
11 /			
12 GTO D			
13♦LBL B	°C-K		
14 273.15			
15 +			
16 GTO D			
17♦LBL C	°R-K	70	
18 1.8			
19 /			
20♦LBL D	K-K		
21 PROMPT			
22♦LBL A	K-°F		
23 1.8			
24 *			
25 459.67			
26 -			
27 GTO 00			
28♦LBL B	K-°C	80	
29 273.15			
30 -			
31 GTO 00			
32♦LBL C	K-°R		
33 1.8			
34 *			
35♦LBL D	K-K		
36 GTO 00			
37 .END.			
40		90	
50		00	

HEWLETT-PACKARD

HP-41C

USERS' LIBRARY SOLUTIONS

Bar Codes

Heating, Ventilating &
Air Conditioning

HEATING, VENTILATING & AIR CONDITIONING

OVERALL HEAT TRANSFER COEFFICIENTS 1
INSULATION BREAK EVEN ANALYSIS 2
AIR FLOW IN CIRCULAR DUCTS 3
AIR DUCT CONVERSION 6
EQUATIONS OF STATE 7
BLACK BODY THERMAL RADIATION 9
PSYCHROMETRIC PROPERTIES 11
HEAT EXCHANGERS 15
DECIBEL ADDITION AND SUBTRACTION 21
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OVERALL HEAT TRANSFER
COEFFICIENTS
PROGRAM REGISTERS NEEDED: 16

HEWLETT PACKARD
SOLUTION BOOK:
HEAT VENT & A/C

ROW 1 (1 - 4)



ROW 2 (5 - 7)



ROW 3 (7 - 14)



ROW 4 (14 - 20)



ROW 5 (21 - 26)



ROW 6 (26 - 33)



ROW 7 (33 - 40)



ROW 8 (41 - 48)



ROW 9 (48 - 50)



INSULATION BREAK EVEN ANALYSIS

HEWLETT PACKARD
SOLUTION BOOK:
HEAT VENT & A/C

PROGRAM REGISTERS NEEDED: 29

ROW 1 (1 - 5)



ROW 2 (5 - 8)



ROW 3 (8 - 11)



ROW 4 (11 - 13)



ROW 5 (14 - 19)



ROW 6 (20 - 24)



ROW 7 (25 - 36)



ROW 8 (37 - 46)



ROW 9 (47 - 57)



ROW 10 (58 - 63)



ROW 11 (64 - 74)



ROW 12 (74 - 79)



ROW 13 (79 - 85)



ROW 14 (86 - 93)



ROW 15 (93 - 98)



ROW 16 (99 - 99)



AIR FLOW IN CIRCULAR DUCTS

HEWLETT PACKARD
SOLUTION BOOK:
HEAT VENT & A/C

PROGRAM REGISTERS NEEDED: 90

ROW 1 (1 - 3)



ROW 2 (4 - 7)



ROW 3 (7 - 13)



ROW 4 (14 - 17)



ROW 5 (18 - 24)



ROW 6 (24 - 30)



ROW 7 (30 - 36)



ROW 8 (37 - 40)



ROW 9 (40 - 44)



ROW 10 (45 - 50)



ROW 11 (50 - 53)



ROW 12 (53 - 57)



ROW 13 (57 - 60)



ROW 14 (60 - 65)



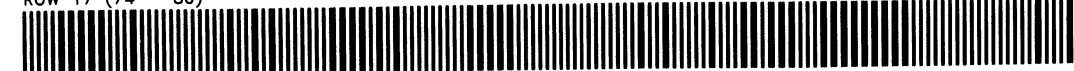
ROW 15 (66 - 71)



ROW 16 (71 - 73)



ROW 17 (74 - 80)



ROW 18 (81 - 87)



ROW 19 (87 - 92)

ROW 20 (92 - 97)

ROW 21 (98 - 105)

ROW 22 (105 - 108)

ROW 23 (109 - 112)

ROW 24 (112 - 117)

ROW 25 (118 - 122)

ROW 26 (123 - 125)

ROW 27 (126 - 129)

ROW 28 (129 - 132)

ROW 29 (132 - 136)

ROW 30 (137 - 143)

ROW 31 (144 - 152)

ROW 32 (153 - 163)

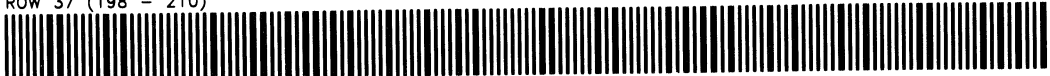
ROW 33 (164 - 169)

ROW 34 (170 - 179)

ROW 35 (180 - 188)

ROW 36 (189 - 197)

ROW 37 (198 - 210)



ROW 38 (211 - 222)



ROW 39 (223 - 231)



ROW 40 (232 - 242)



ROW 41 (243 - 250)



ROW 42 (250 - 252)



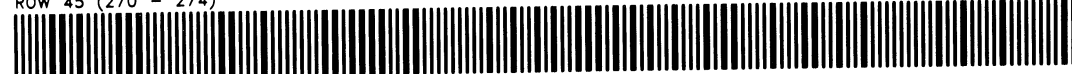
ROW 43 (252 - 259)



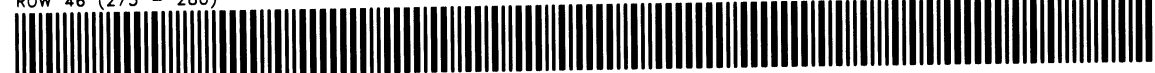
ROW 44 (260 - 269)



ROW 45 (270 - 274)



ROW 46 (275 - 280)



ROW 47 (281 - 288)



ROW 48 (289 - 293)



ROW 49 (294 - 295)



AIR DUCT CONVERSION

PROGRAM REGISTERS NEEDED: 33

HEWLETT PACKARD
SOLUTION BOOK:
HEAT VENT & A/C

ROW 1 (1 - 3)



ROW 2 (4 - 9)



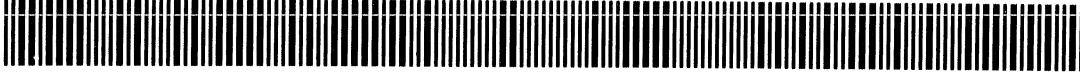
ROW 3 (9 - 18)



ROW 4 (19 - 27)



ROW 5 (27 - 29)



ROW 6 (29 - 36)



ROW 7 (36 - 44)



ROW 8 (45 - 54)



ROW 9 (54 - 65)



ROW 10 (65 - 71)



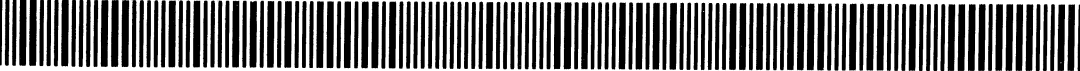
ROW 11 (71 - 77)



ROW 12 (78 - 88)



ROW 13 (88 - 96)



ROW 14 (96 - 101)



ROW 15 (101 - 106)



ROW 16 (107 - 114)



ROW 17 (115 - 120)



ROW 18 (120 - 123)



EQUATIONS OF STATE

HEWLETT PACKARD
SOLUTION BOOK:
HEAT VENT & A/C

PROGRAM REGISTERS NEEDED: 47

ROW 1 (1 - 5)



ROW 2 (5 - 10)



ROW 3 (11 - 17)



ROW 4 (18 - 24)



ROW 5 (25 - 30)



ROW 6 (30 - 37)



ROW 7 (38 - 47)



ROW 8 (48 - 55)



ROW 9 (55 - 65)



ROW 10 (66 - 73)



ROW 11 (73 - 79)



ROW 12 (80 - 91)



ROW 13 (91 - 98)



ROW 14 (98 - 108)



ROW 15 (109 - 121)



ROW 16 (122 - 130)



ROW 17 (130 - 138)



ROW 18 (139 - 151)



ROW 19 (152 - 164)



ROW 20 (165 - 177)



ROW 21 (178 - 190)



ROW 22 (191 - 202)



ROW 23 (203 - 210)



ROW 24 (211 - 222)



ROW 25 (222 - 230)



ROW 26 (230 - 230)



BLACK BODY THERMAL RADIATION

PROGRAM REGISTERS NEEDED: 50

HEWLETT PACKARD
SOLUTION BOOK:
HEAT VENT & A/C

ROW 1 (1 - 4)



ROW 2 (4 - 10)



ROW 3 (10 - 13)



ROW 4 (13 - 17)



ROW 5 (17 - 20)



ROW 6 (20 - 23)



ROW 7 (23 - 27)



ROW 8 (27 - 30)



ROW 9 (30 - 33)



ROW 10 (33 - 36)



ROW 11 (36 - 42)



ROW 12 (42 - 49)



ROW 13 (49 - 52)



ROW 14 (53 - 58)



ROW 15 (58 - 61)



ROW 16 (62 - 74)



ROW 17 (75 - 82)



ROW 18 (83 - 94)



ROW 19 (95 - 107)



ROW 20 (108 - 120)



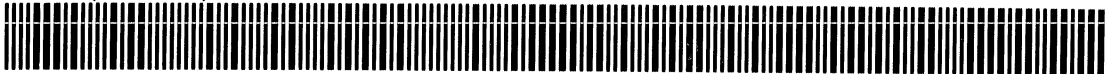
ROW 21 (121 - 131)



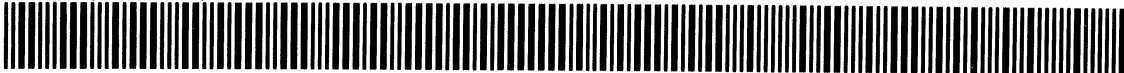
ROW 22 (131 - 140)



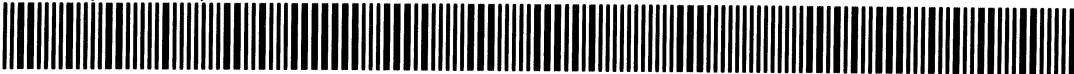
ROW 23 (141 - 146)



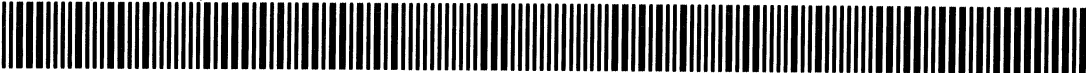
ROW 24 (146 - 149)



ROW 25 (149 - 157)



ROW 26 (158 - 167)



ROW 27 (167 - 170)



PSYCHROMETRIC PROPERTIES

HEWLETT PACKARD
SOLUTION BOOK:
HEAT VENT & A/C

PROGRAM REGISTERS NEEDED: 129

ROW 1 (1 : 2)



ROW 2 (3 : 5)



ROW 3 (5 : 12)



ROW 4 (12 : 16)



ROW 5 (16 : 20)



ROW 6 (20 : 25)



ROW 7 (25 : 27)



ROW 8 (27 : 33)



ROW 9 (33 : 37)



ROW 10 (37 : 40)



ROW 11 (41 : 45)



ROW 12 (46 : 47)



ROW 13 (48 : 56)



ROW 14 (56 : 59)



ROW 15 (60 : 65)



ROW 16 (66 : 74)



ROW 17 (75 : 80)



ROW 18 (80 : 85)



ROW 19 (86 : 91)



ROW 20 (91 : 97)



ROW 21 (98 : 106)



ROW 22 (107 : 112)



ROW 23 (113 : 120)



ROW 24 (121 : 126)



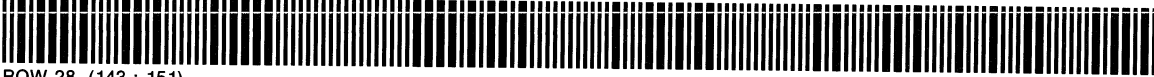
ROW 25 (126 : 130)



ROW 26 (131 : 138)



ROW 27 (139 : 143)



ROW 28 (143 : 151)



ROW 29 (151 : 153)



ROW 30 (153 : 161)



ROW 31 (162 : 170)



ROW 32 (170 : 177)



ROW 33 (177 : 184)



ROW 34 (184 : 186)



ROW 35 (186 : 191)



ROW 36 (191 : 193)



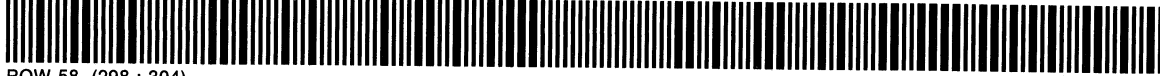
ROW 55 (275 : 285)



ROW 56 (286 : 289)



ROW 57 (290 : 298)



ROW 58 (298 : 304)



ROW 59 (305 : 309)



ROW 60 (310 : 314)



ROW 61 (314 : 321)



ROW 62 (322 : 328)



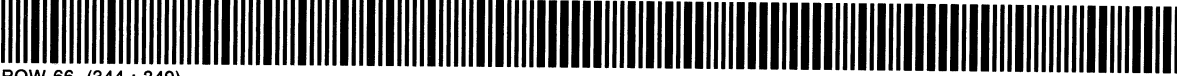
ROW 63 (328 : 332)



ROW 64 (332 : 335)



ROW 65 (336 : 344)



ROW 66 (344 : 349)



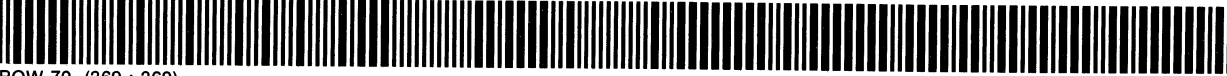
ROW 67 (349 : 355)



ROW 68 (356 : 363)



ROW 69 (363 : 368)



ROW 70 (369 : 369)



HEAT EXCHANGERS

HEWLETT PACKARD
SOLUTION BOOK:
HEAT VENT & A/C

PROGRAM REGISTERS NEEDED: 67

ROW 1 (1 - 4)



ROW 2 (4 - 6)



ROW 3 (6 - 11)



ROW 4 (11 - 14)



ROW 5 (15 - 20)



ROW 6 (20 - 26)



ROW 7 (27 - 33)



ROW 8 (33 - 34)



ROW 9 (35 - 40)



ROW 10 (40 - 44)



ROW 11 (45 - 51)



ROW 12 (51 - 57)



ROW 13 (57 - 64)



ROW 14 (64 - 70)



ROW 15 (70 - 75)



ROW 16 (76 - 81)



ROW 17 (81 - 88)



ROW 18 (88 - 94)



ROW 19 (94 - 102)

ROW 20 (103 - 110)

ROW 21 (111 - 119)

ROW 22 (119 - 129)

ROW 23 (130 - 137)

ROW 24 (138 - 148)

ROW 25 (149 - 161)

ROW 26 (162 - 168)

ROW 27 (168 - 175)

ROW 28 (176 - 183)

ROW 29 (184 - 196)

ROW 30 (197 - 203)

ROW 31 (204 - 206)

ROW 32 (206 - 210)

ROW 33 (211 - 216)

ROW 34 (217 - 224)

ROW 35 (225 - 230)

ROW 36 (231 - 234)

HEAT EXCHANGERS:
PARALLEL FLOW SUBROUTINE
PROGRAM REGISTERS NEEDED: 8

HEWLETT PACKARD
SOLUTION BOOK:
HEAT VENT & A/C

ROW 1 (1 - 6)



ROW 2 (7 - 19)



ROW 3 (19 - 25)



ROW 4 (26 - 36)



HEAT EXCHANGERS:
COUNTER FLOW SUBROUTINE
PROGRAM REGISTERS NEEDED: 11

HEWLETT PACKARD
SOLUTION BOOK:
HEAT VENT & A/C

ROW 1 (1 - 6)



ROW 2 (7 - 18)



ROW 3 (19 - 28)



ROW 4 (28 - 37)



ROW 5 (38 - 49)



ROW 6 (50 - 59)



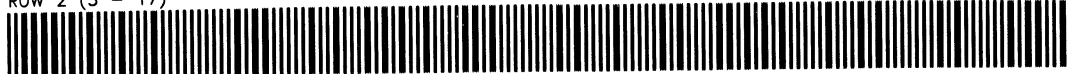
HEAT EXCHANGERS:
PARALLEL-COUNTER FLOW SUBR.
PROGRAM REGISTERS NEEDED: 12

HEWLETT PACKARD
SOLUTION BOOK:
HEAT VENT & A/C

ROW 1 (1 - 4)



ROW 2 (5 - 17)



ROW 3 (18 - 26)



ROW 4 (26 - 34)



ROW 5 (35 - 47)



ROW 6 (48 - 60)



ROW 7 (61 - 62)



HEAT EXCHANGERS:
CROSS FLOW SUBROUTINE
PROGRAM REGISTERS NEEDED: 14

HEWLETT PACKARD
SOLUTION BOOK:
HEAT VENT & A/C

ROW 1 (1 - 5)



ROW 2 (6 - 14)



ROW 3 (14 - 22)



ROW 4 (22 - 30)



ROW 5 (30 - 35)



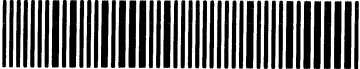
ROW 6 (35 - 44)



ROW 7 (45 - 57)



ROW 8 (57 - 57)



DECIBEL ADDITION AND
SUBTRACTION
PROGRAM REGISTERS NEEDED: 8

HEWLETT PACKARD
SOLUTION BOOK:
HEAT VENT & A/C

ROW 1 (1 - 4)



ROW 2 (5 - 9)



ROW 3 (10 - 16)



ROW 4 (17 - 26)



ROW 5 (26 - 26)



TEMPERATURE CONVERSION

PROGRAM REGISTERS NEEDED: 15

HEWLETT PACKARD
SOLUTION BOOK:
HEAT VENT & A/C

ROW 1 (1 - 5)



ROW 2 (5 - 7)



ROW 3 (8 - 12)



ROW 4 (12 - 16)



ROW 5 (17 - 23)



ROW 6 (23 - 28)



ROW 7 (29 - 33)



ROW 8 (33 - 37)



NOTES

NOTES

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NOTES



Rev. C

Hewlett-Packard Software

In terms of power and flexibility, the problem-solving potential of the HP-41C programmable calculator is nearly limitless. And in order to see the practical side of this potential, HP has different types of software to help save you time and programming effort. Every one of our software solutions has been carefully selected to effectively increase your problem-solving potential. Chances are, we already have the solutions you're looking for.

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Circuit Analysis
Financial Decisions
Mathematics**

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Surveying
Securities
Statistics
Stress Analysis
Games**

**Home Management
Machine Design
Navigation
Real Estate
Thermal and Transport Science**

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Lending, Saving and Leasing
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Small Business
Geometry
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Test Statistics
Antennas
Chemical Engineering
Control Systems
Electrical Engineering
Fluid Dynamics and Hydraulics**

**Civil Engineering
Heating, Ventilating & Air Conditioning
Mechanical Engineering
Solar Engineering
Calendars
Cardiac/Pulmonary
Chemistry
Games
Optometry I (General)
Optometry II (Contact Lens)
Physics
Surveying**

* Some books require additional memory modules to accommodate all programs.

HEATING, VENTILATING & AIR CONDITIONING

OVERALL HEAT TRANSFER COEFFICIENT
INSULATION BREAK EVEN ANALYSIS
AIR FLOW IN CIRCULAT DUCTS
AIR DUCT CONVERSION
EQUATIONS OF STATE
BLACK BODY THERMAL RADIATION
PSYCHROMETRIC PROPERTIES
HEAT EXCHANGERS
DECIBEL ADDITION AND SUBTRACTION
TEMPERATURE CONVERSIONS

